

Reflection Models I: Ideal Materials

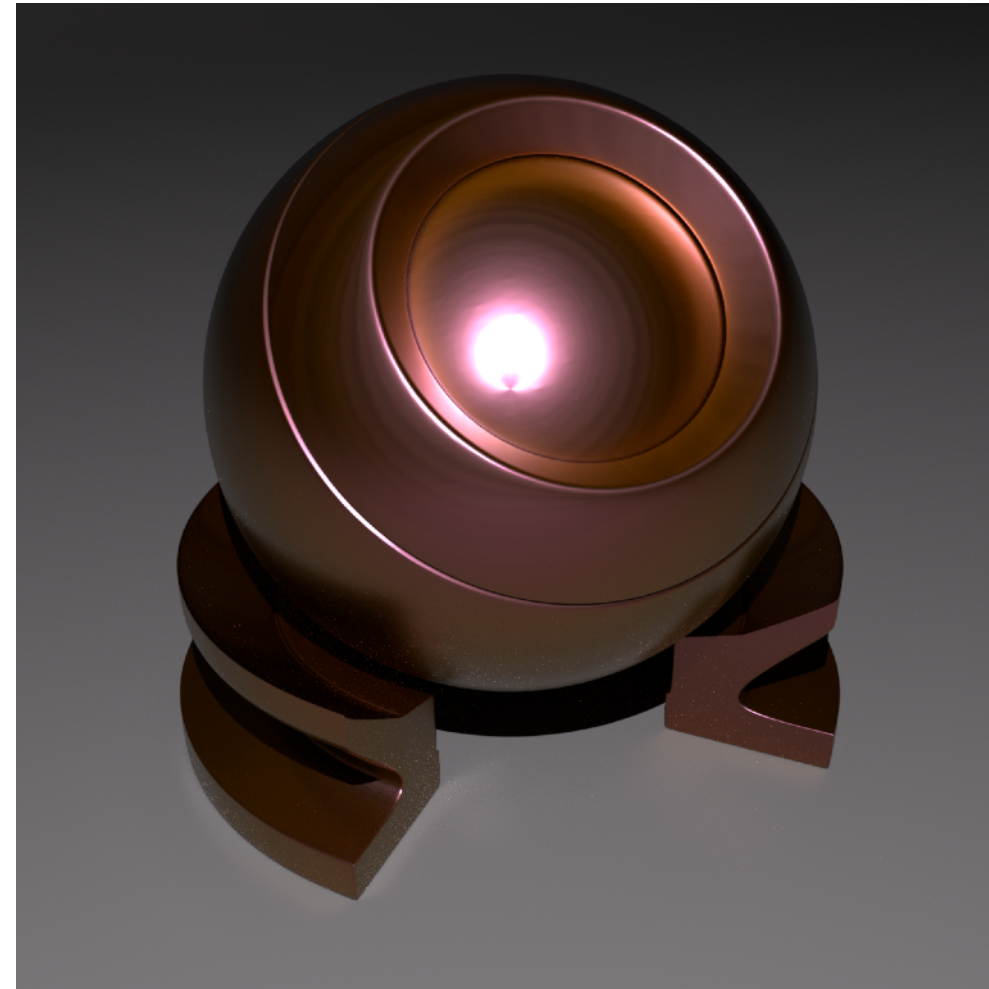
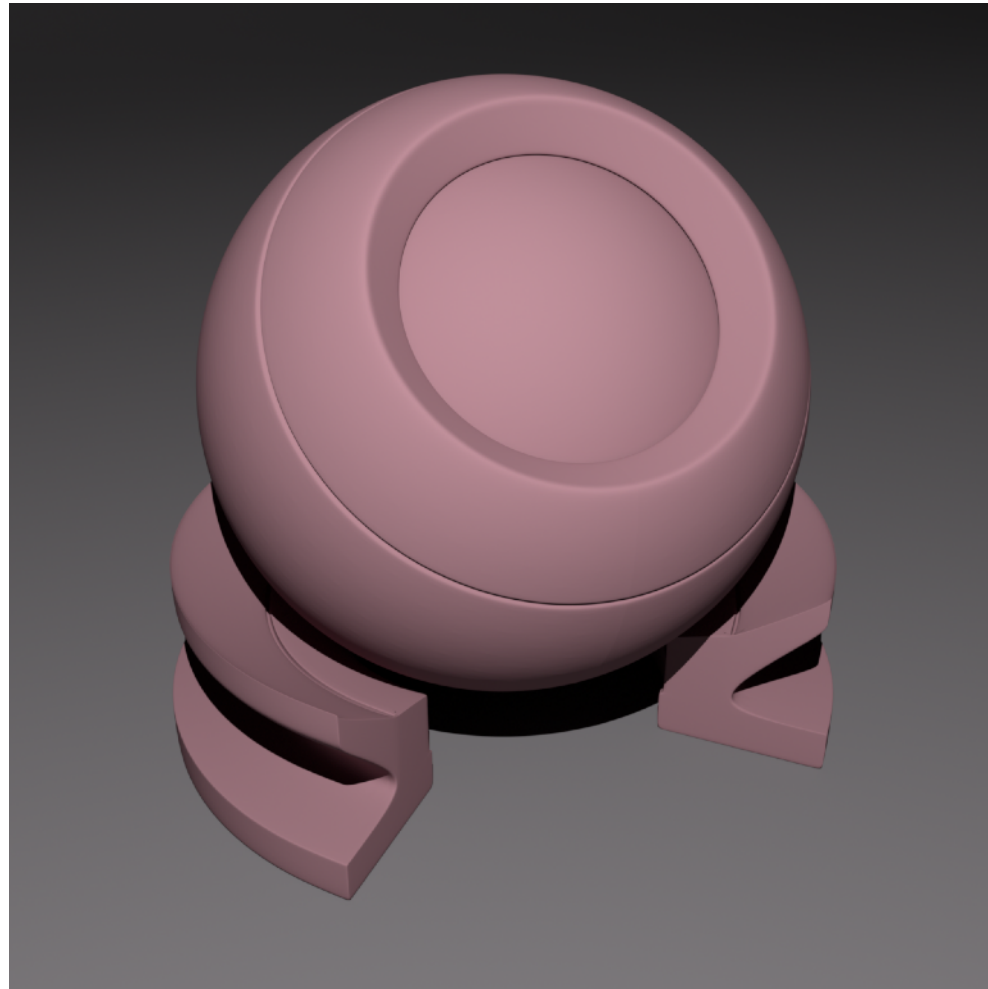
Today

- **The reflection equation**
- **The BRDF and reflectance**
- **Types of reflection models**
- **Ideal reflection and refraction**
- **Fresnel effect**
- **Diffuse reflection**

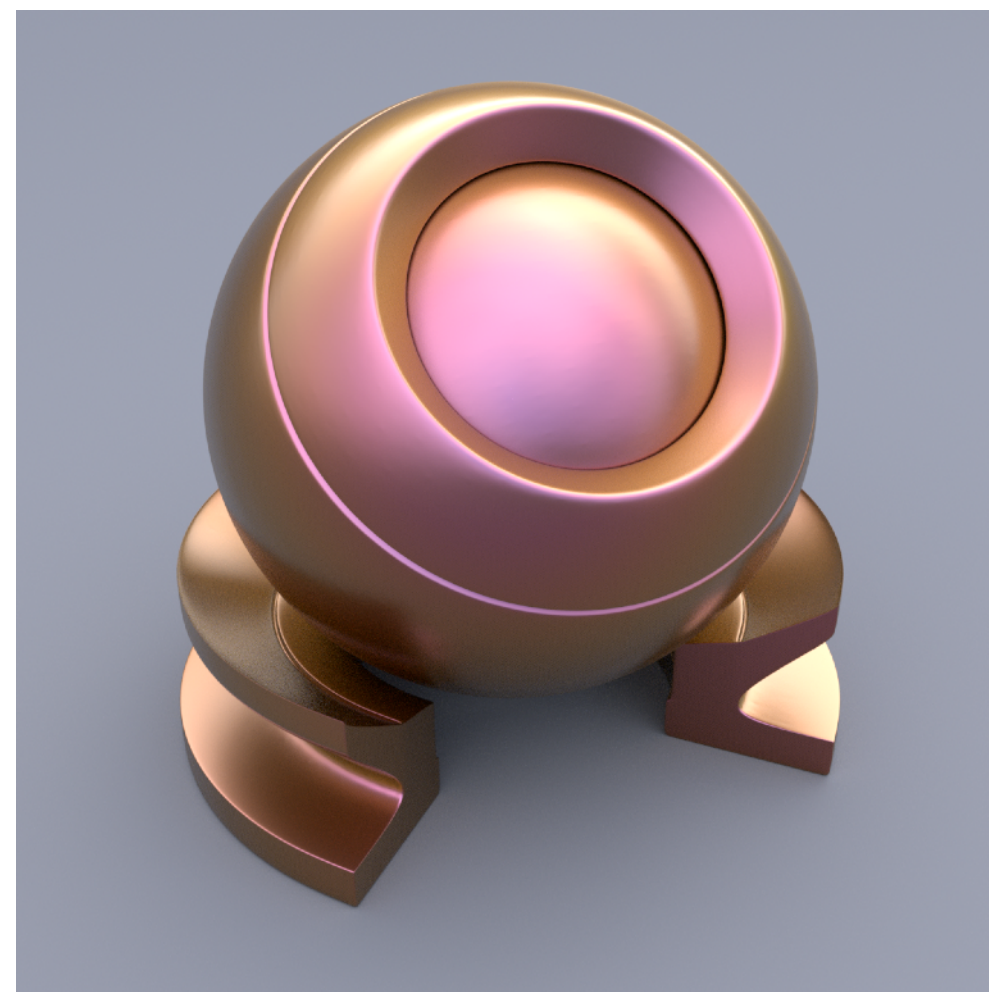
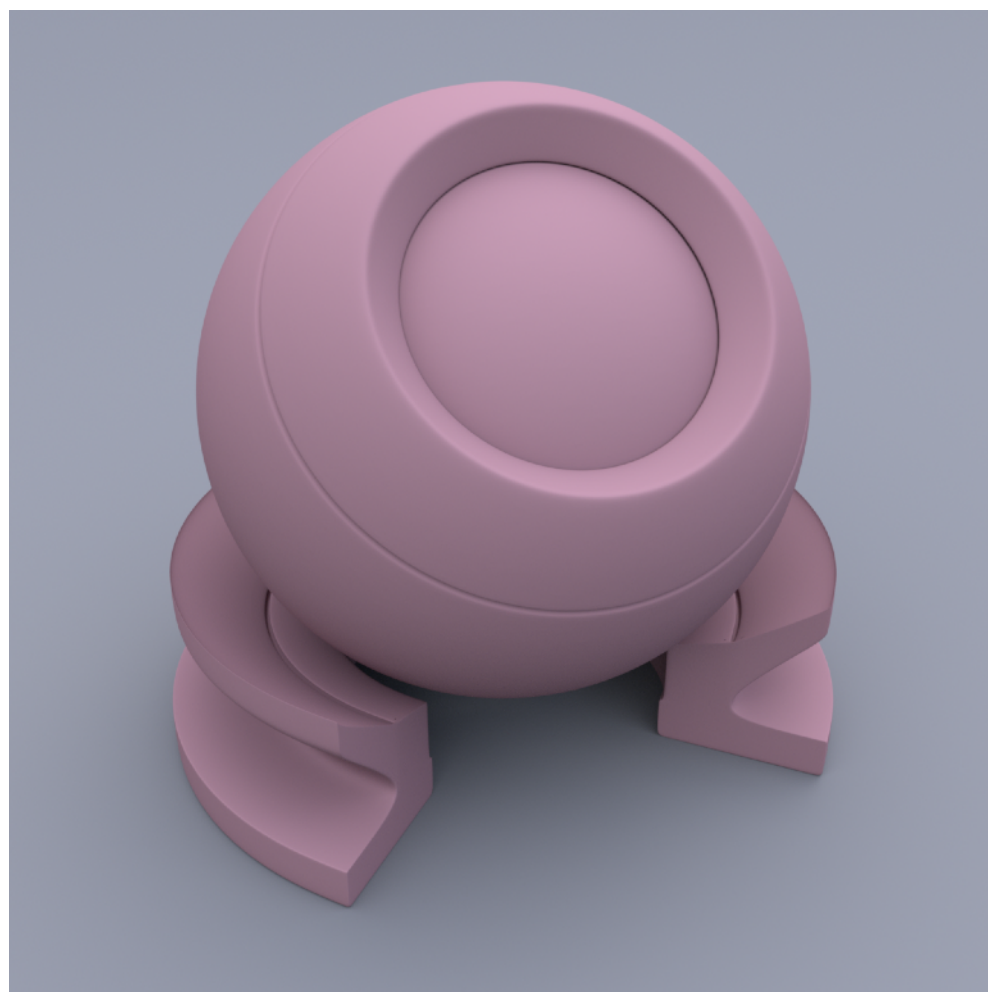
Next lecture

- **Rough surfaces and microfacet distributions**

Surface Appearance



Illumination



Reflection

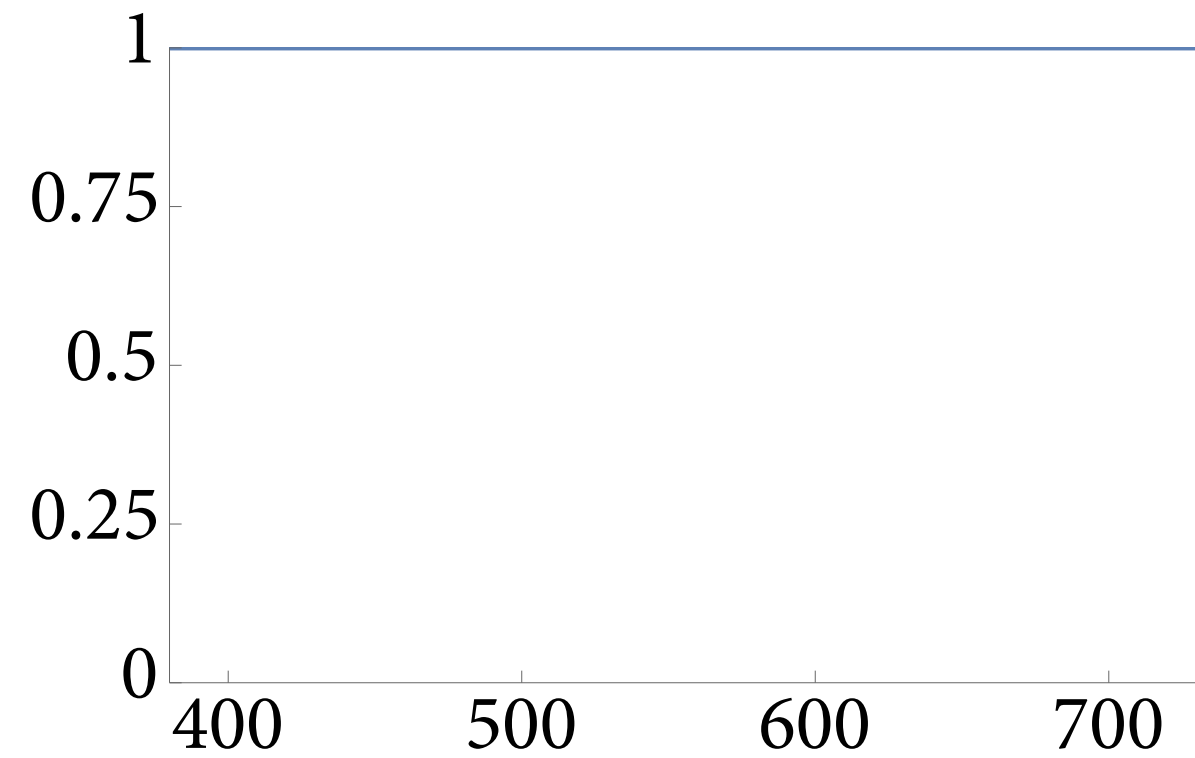
Reflection Models

Definition: Reflection is the process by which light incident on a surface interacts with the surface such that it leaves on the incident side without change in frequency.

Properties

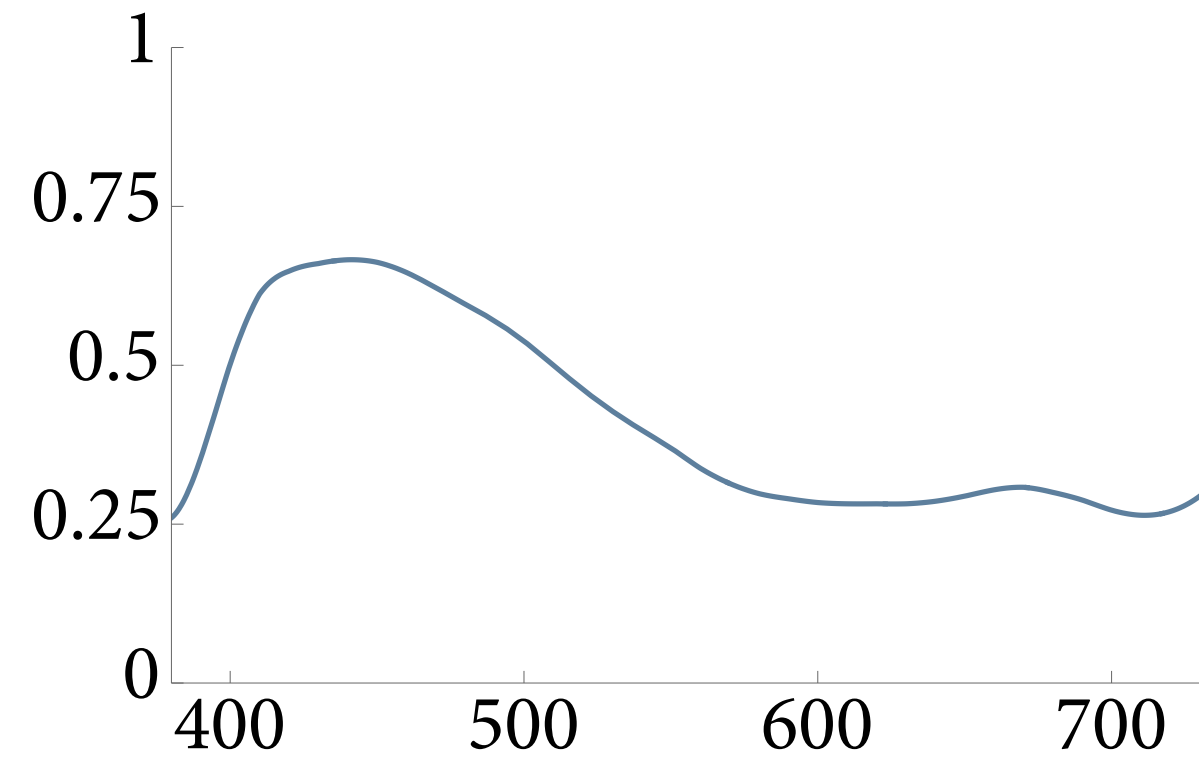
- **Spectral distribution**
- **Polarization**
- **Directional distribution**

Spectral Reflection

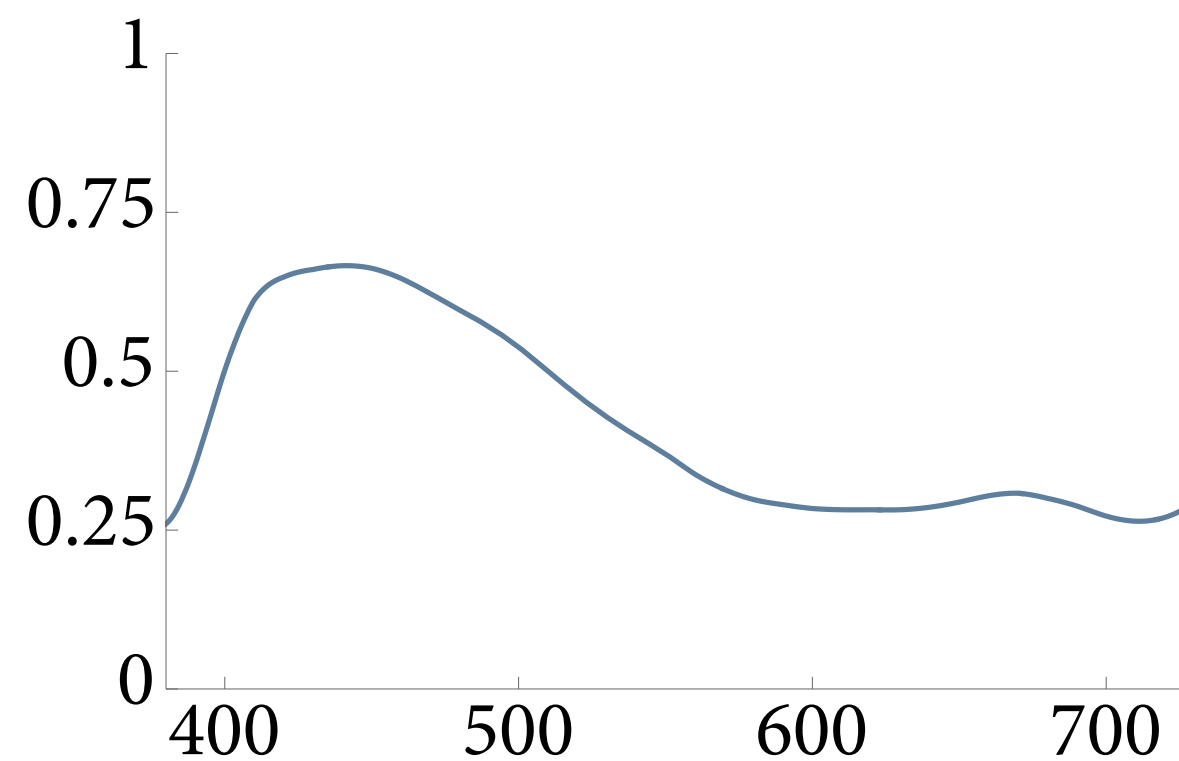
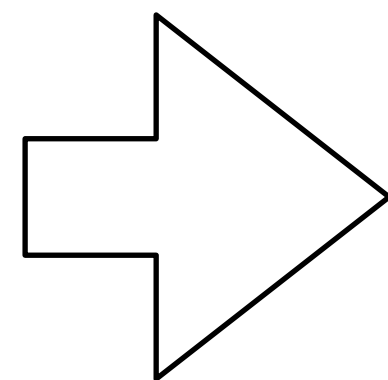


Illumination

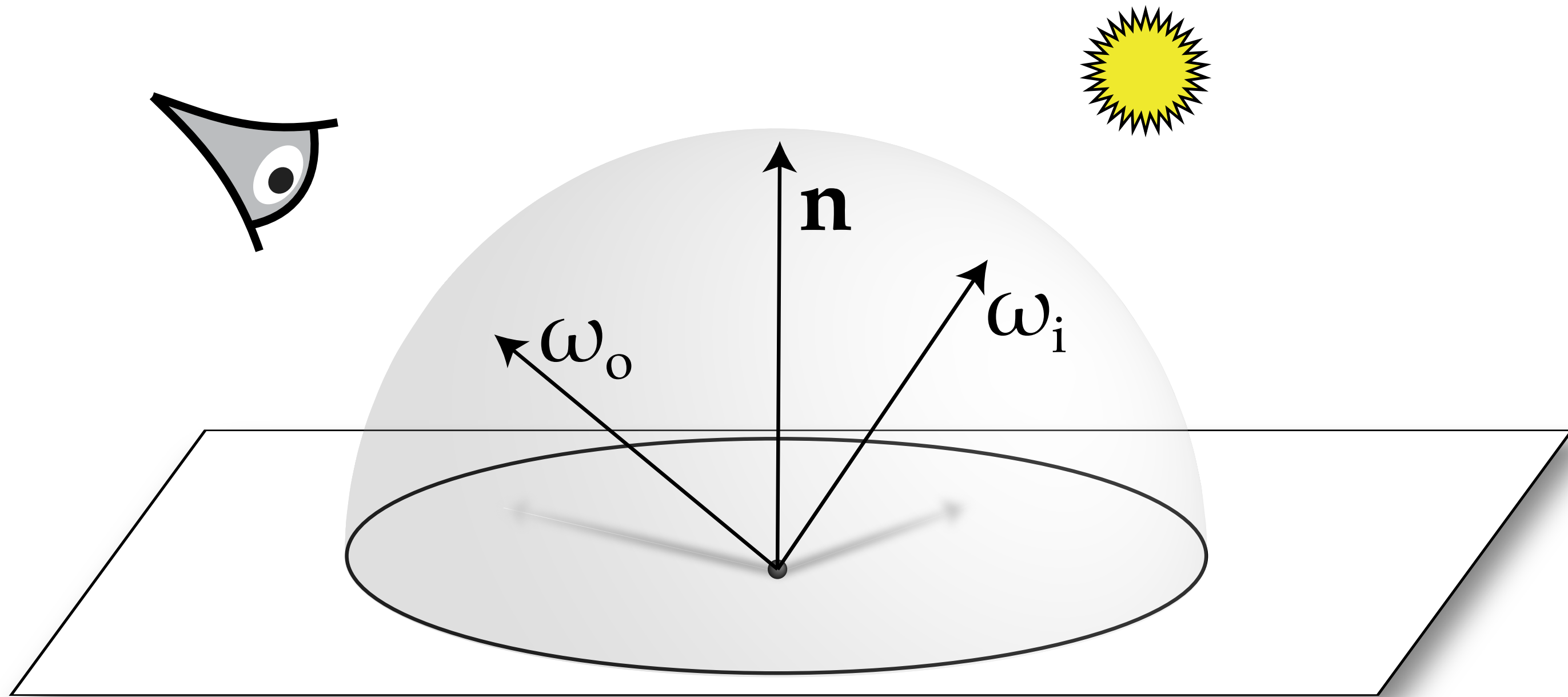
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Reflection



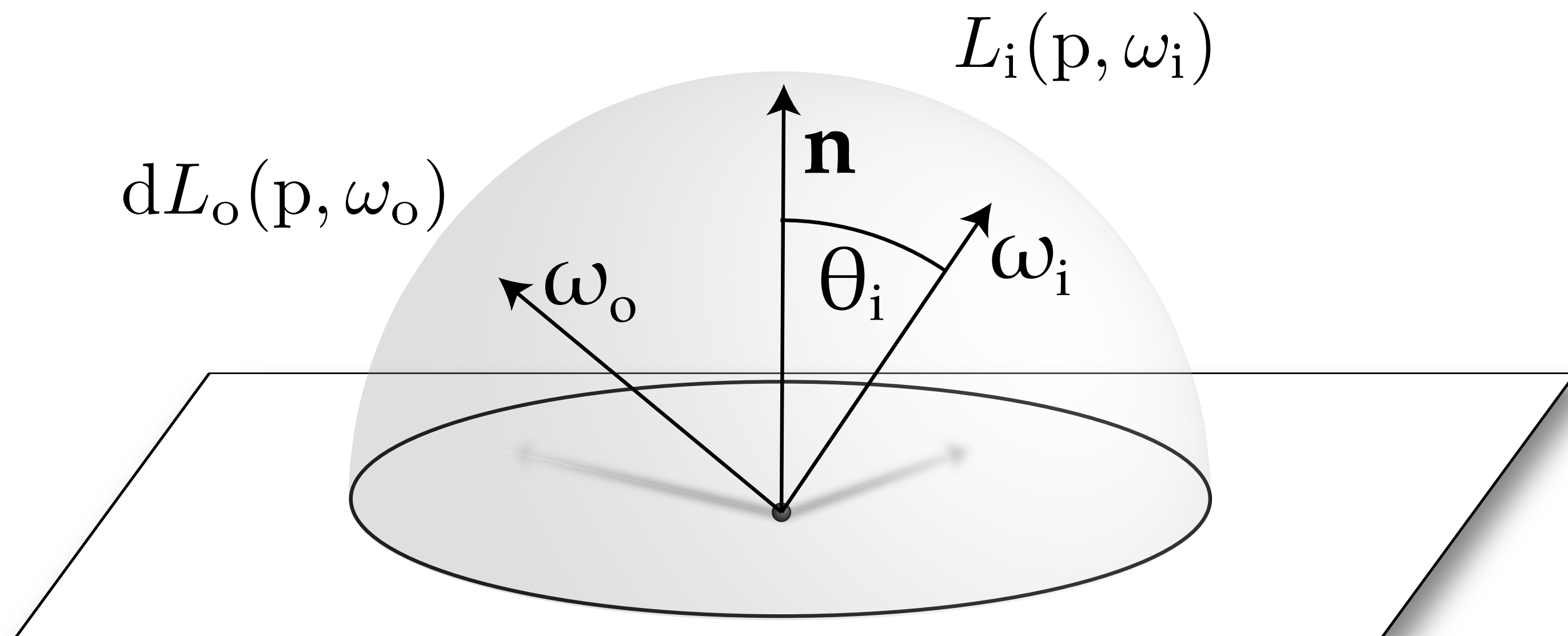
The Reflection Equation



$$L_o(p, \omega_o) = \int_{\Omega^2} \underbrace{f_r(p, \omega_i \rightarrow \omega_o)}_{\text{BRDF}} \underbrace{L_i(p, \omega_i) \cos \theta_i}_{\text{Illumination}} d\omega_i$$

The BRDF

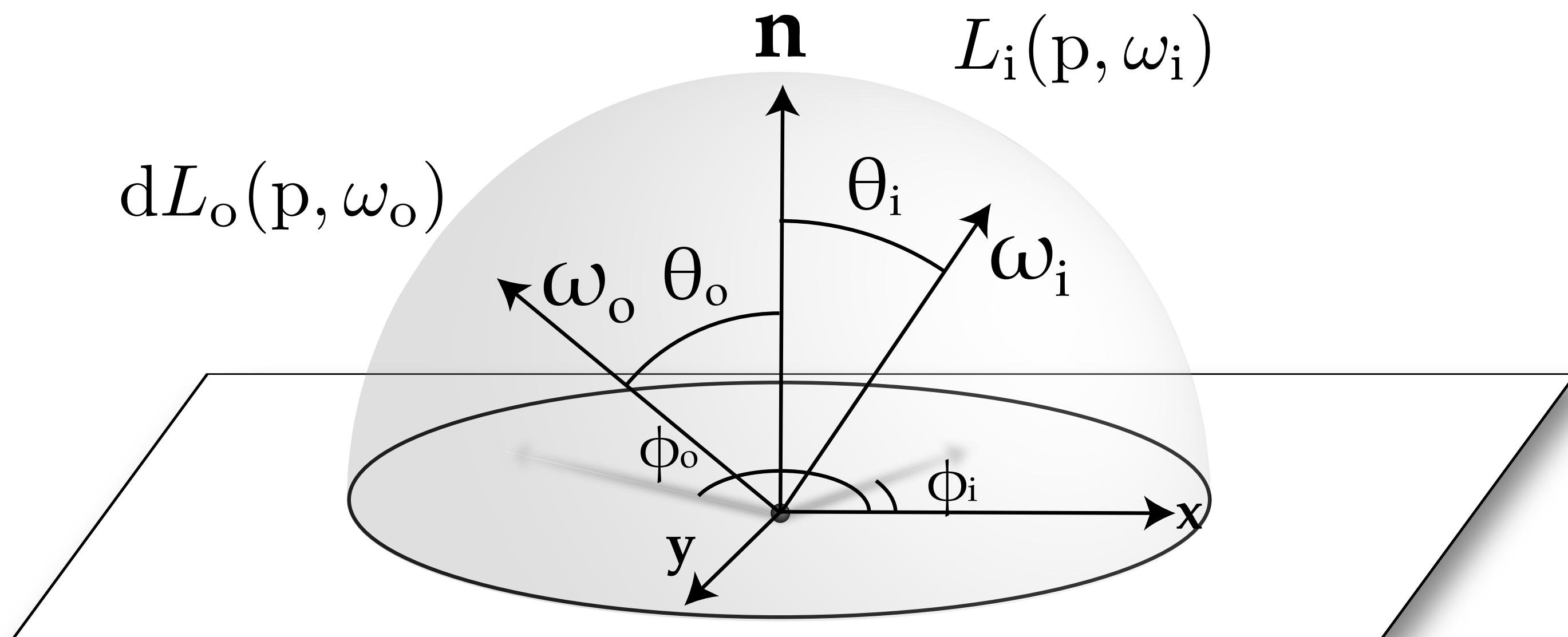
Bidirectional Reflectance-Distribution Function



$$f_r(\omega_i \rightarrow \omega_o) \equiv \frac{dL_o(\omega_o)}{dE_i(\omega_i)} \left[\frac{1}{sr} \right]$$

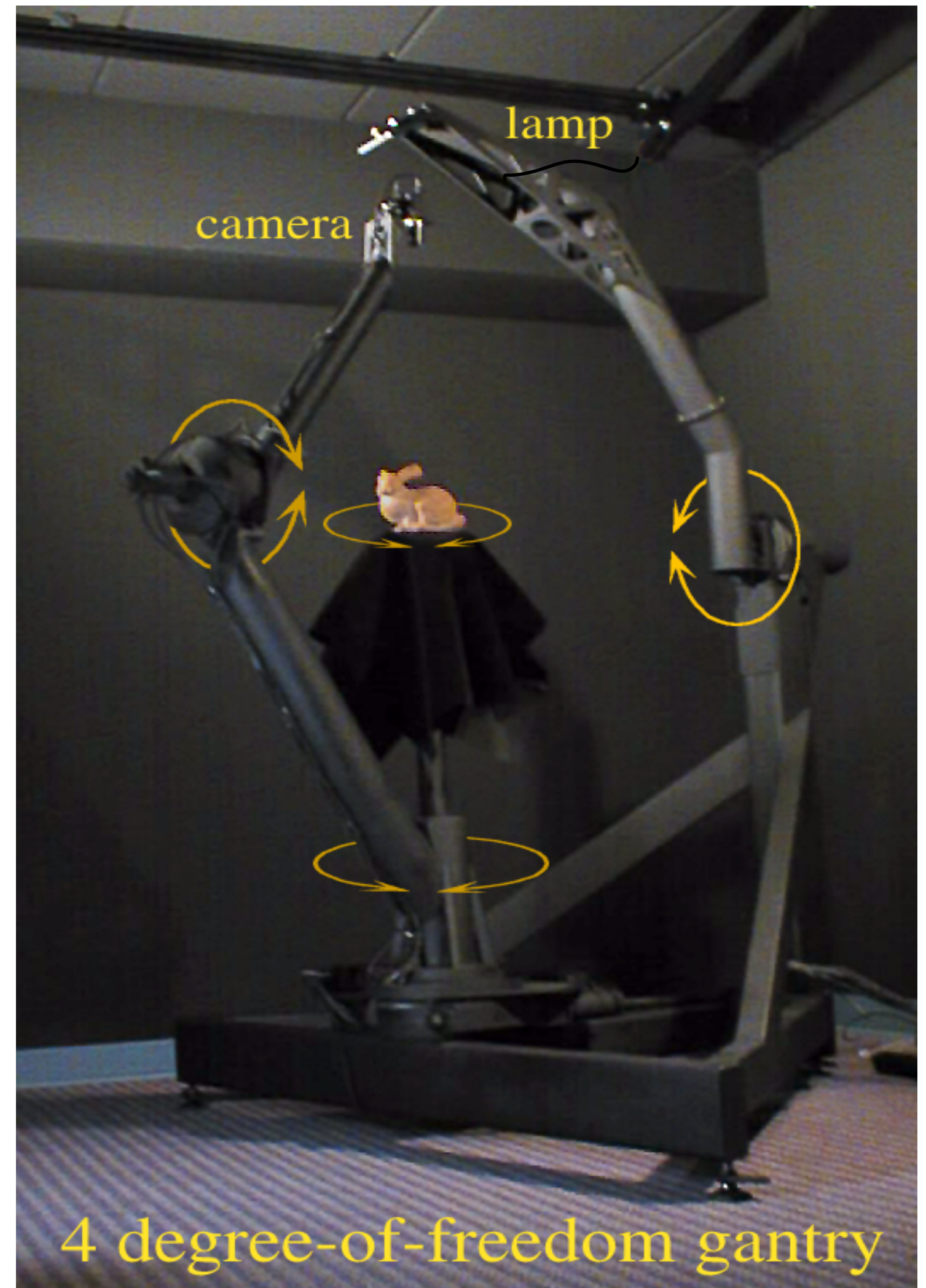
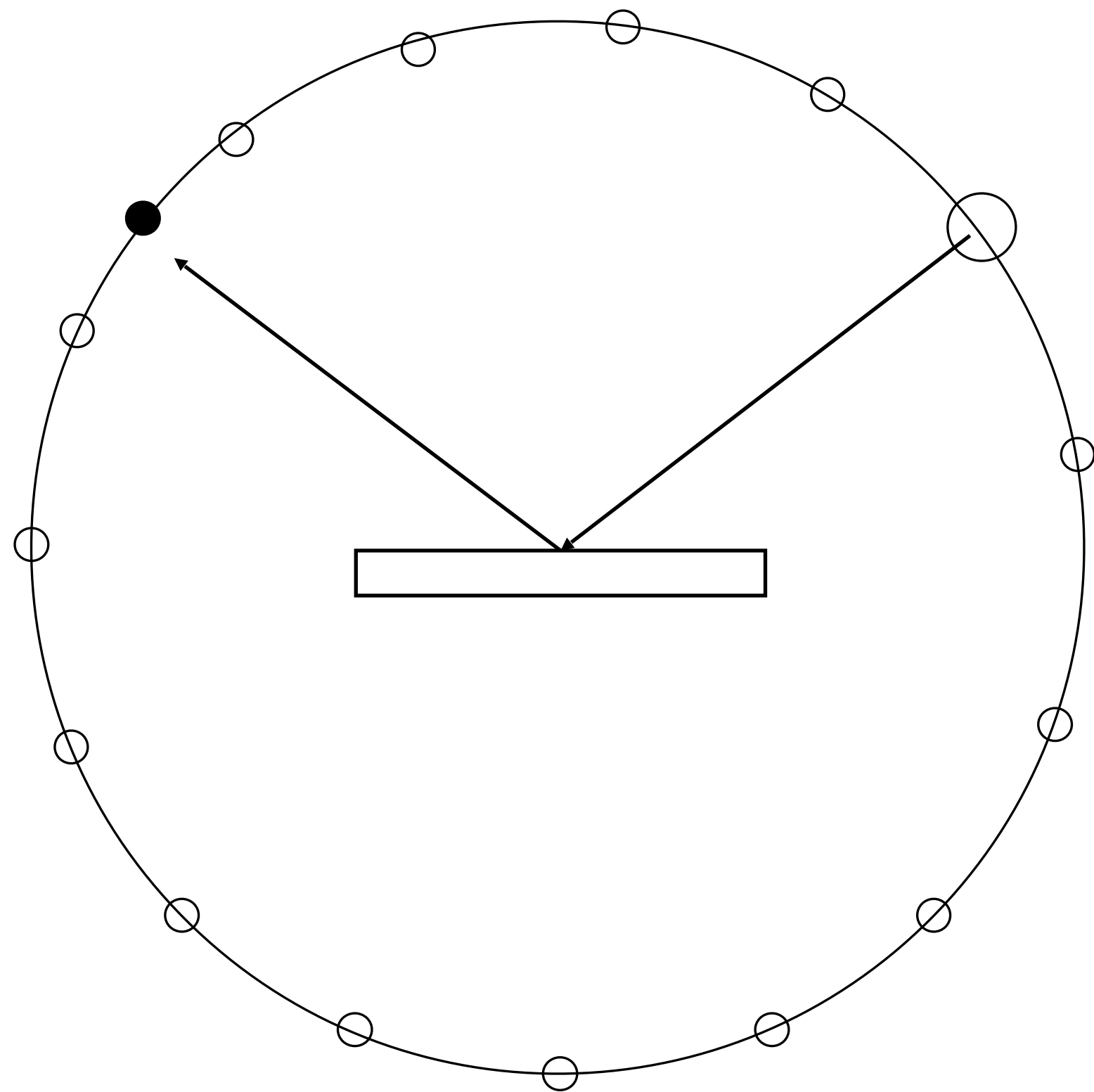
The BRDF

Bidirectional Reflectance-Distribution Function

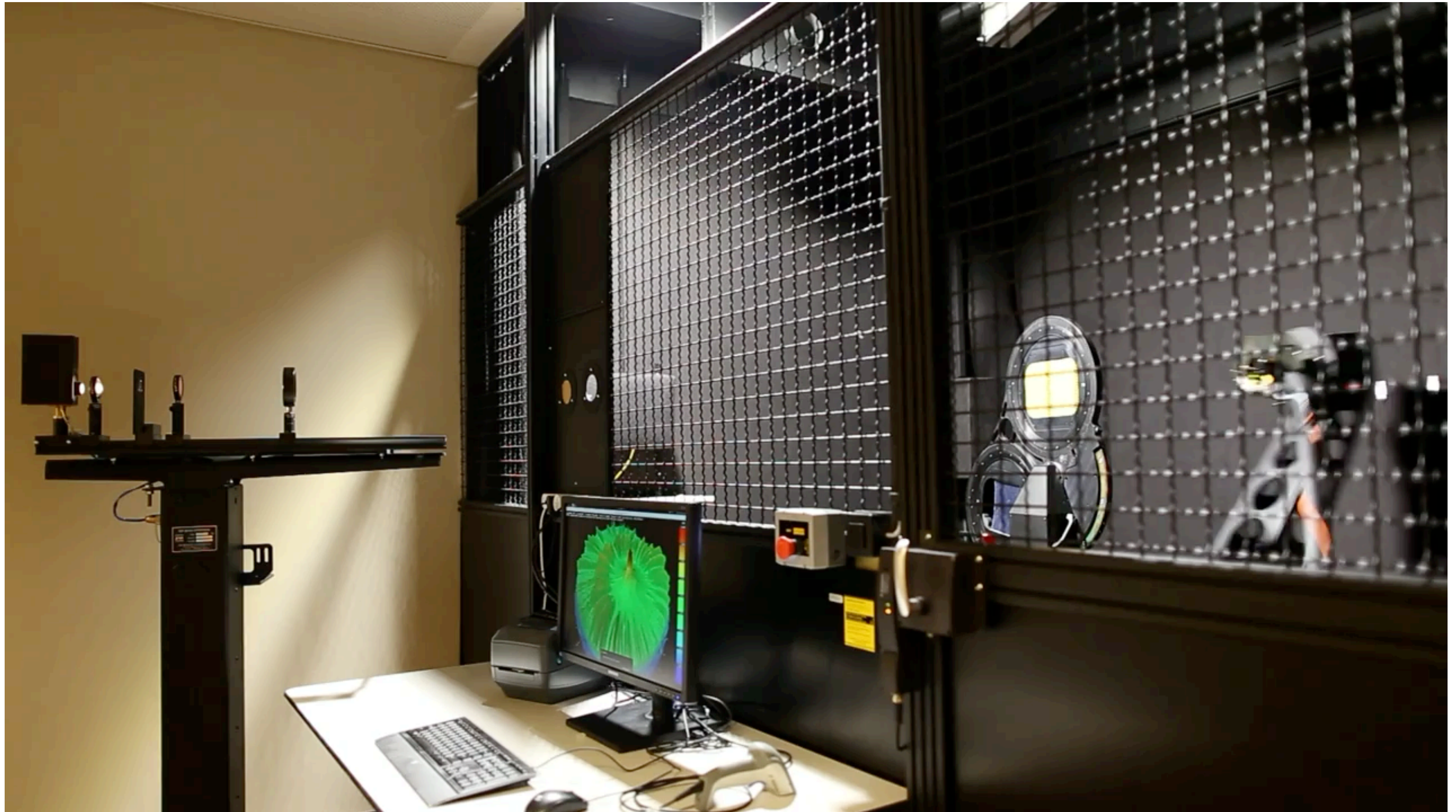


$$f_r(\omega_i \rightarrow \omega_o) \equiv \frac{dL_o(\omega_o)}{dE_i(\omega_i)} \left[\frac{1}{sr} \right]$$

Stanford Gonioreflectometer

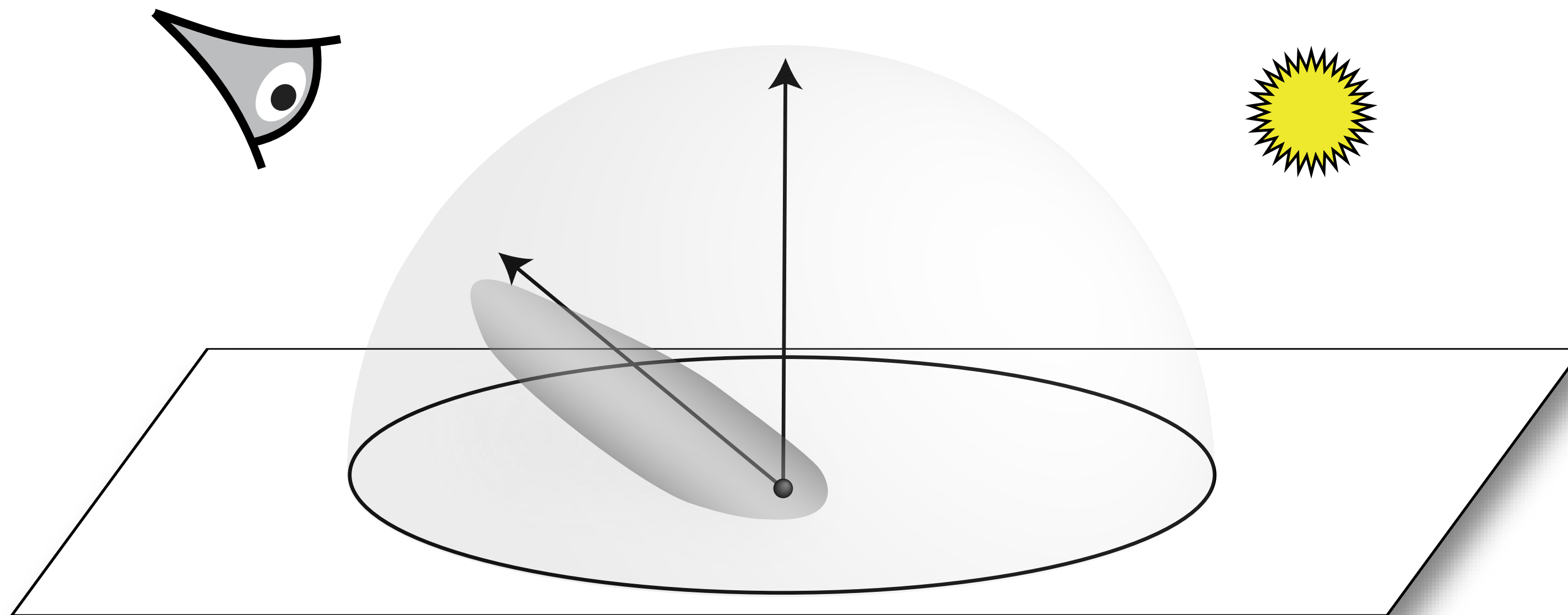


EPFL Gonioreflectometer



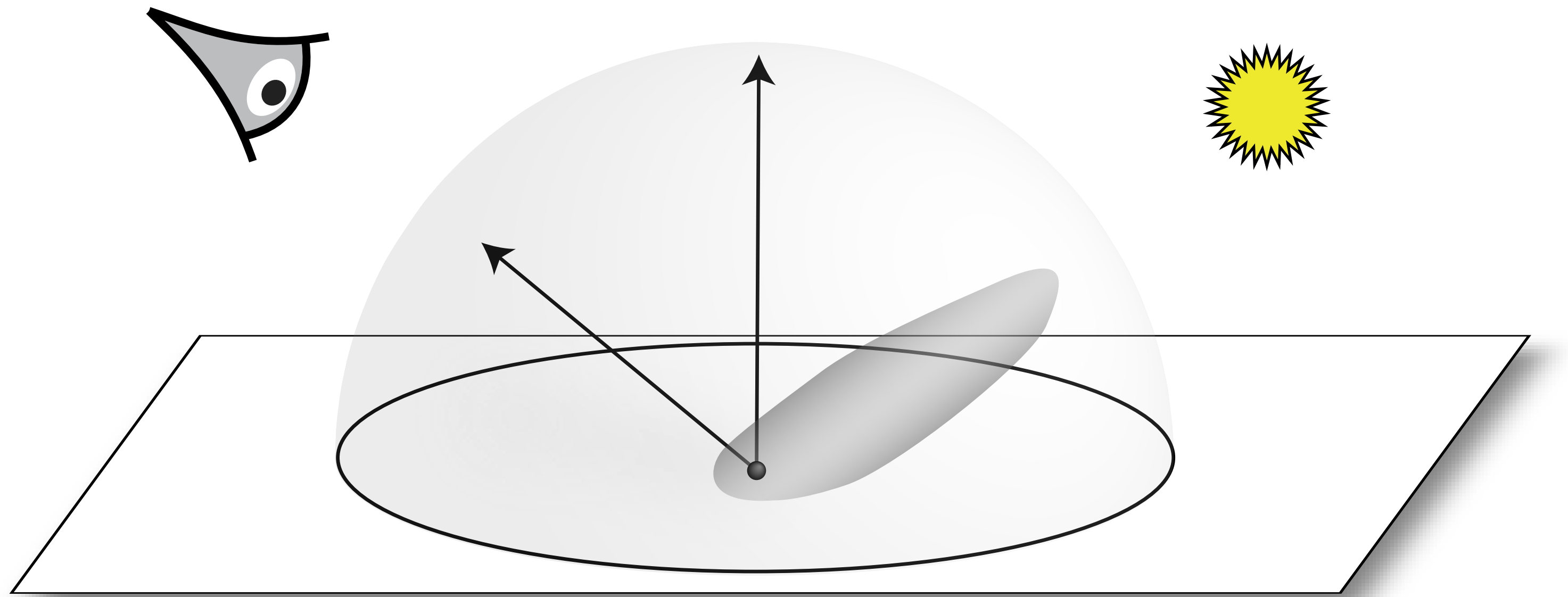
2D Slices of the BRDF: Eye

Fix lighting and vary viewing direction



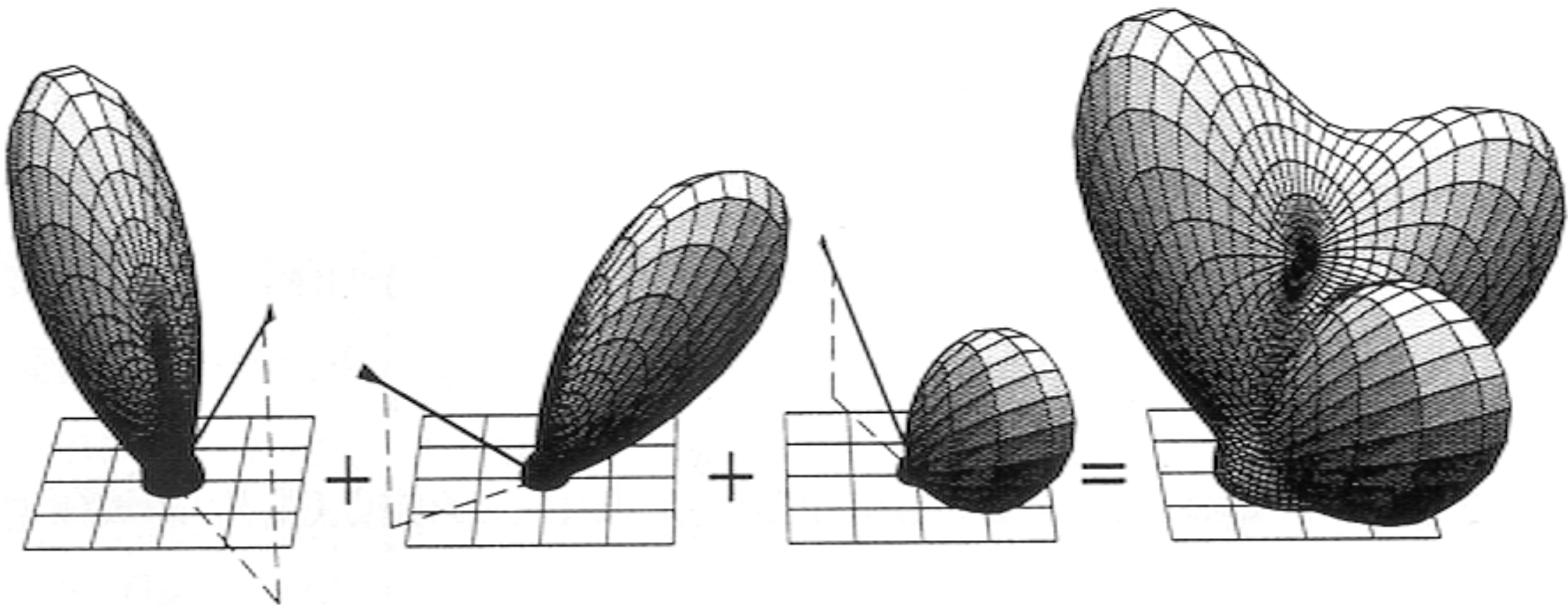
2D Slices of the BRDF: Lighting

Fix viewing direction and vary lighting



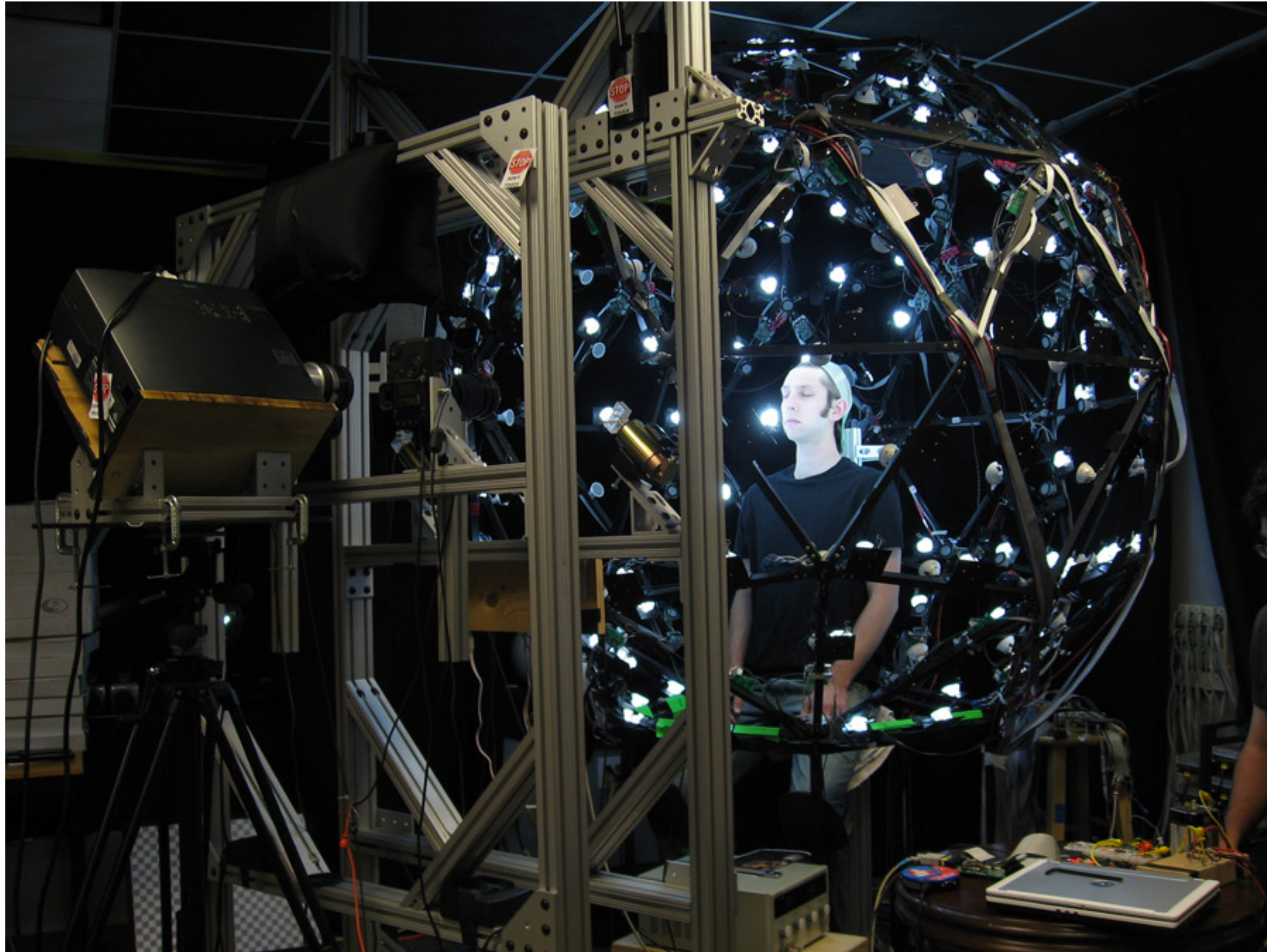
Properties of BRDFs

1. Linearity



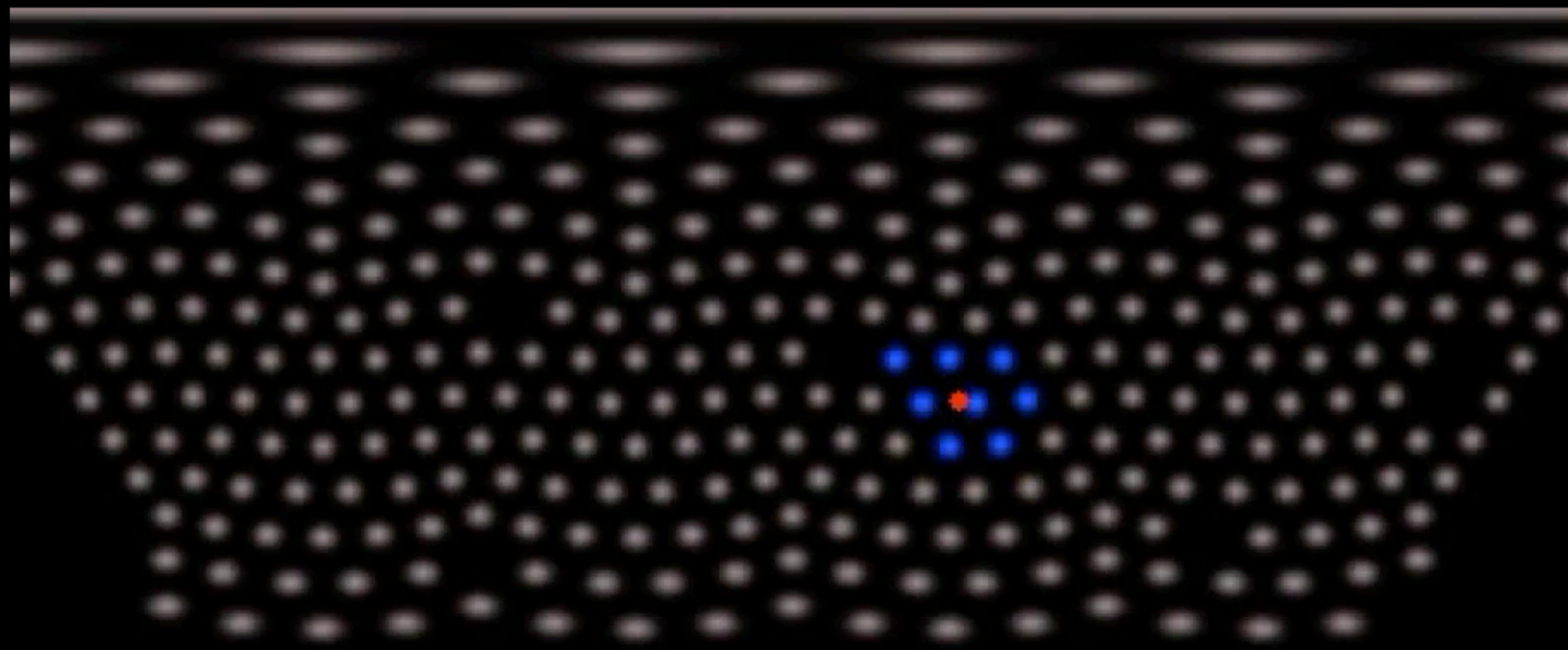
From Sillion, Arvo, Westin, Greenberg

The Light Stage



Leveraging BRDF Linearity: Relighting

Precise Directional Light Relighting



Lights on Light Stage

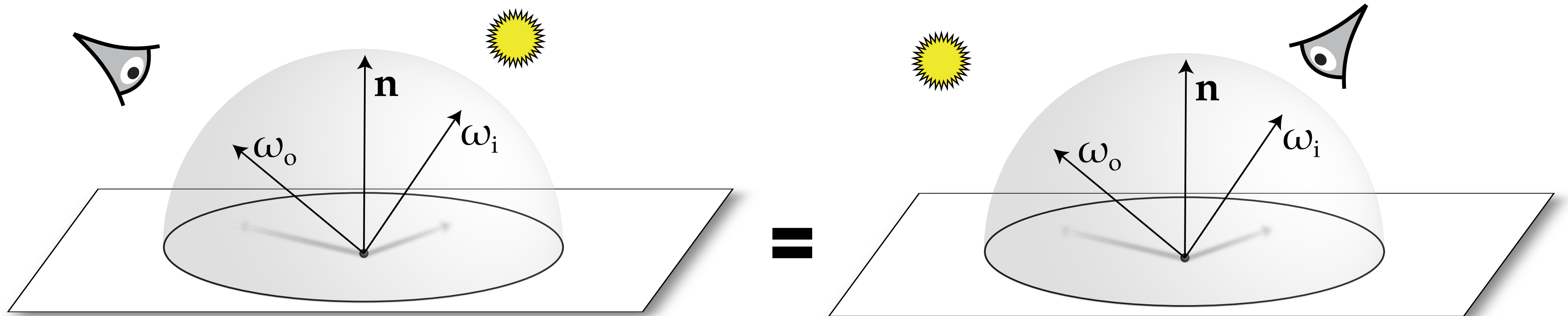


Ours

[Sun et al. 2020]

Properties of BRDFs

2. Reciprocity principle



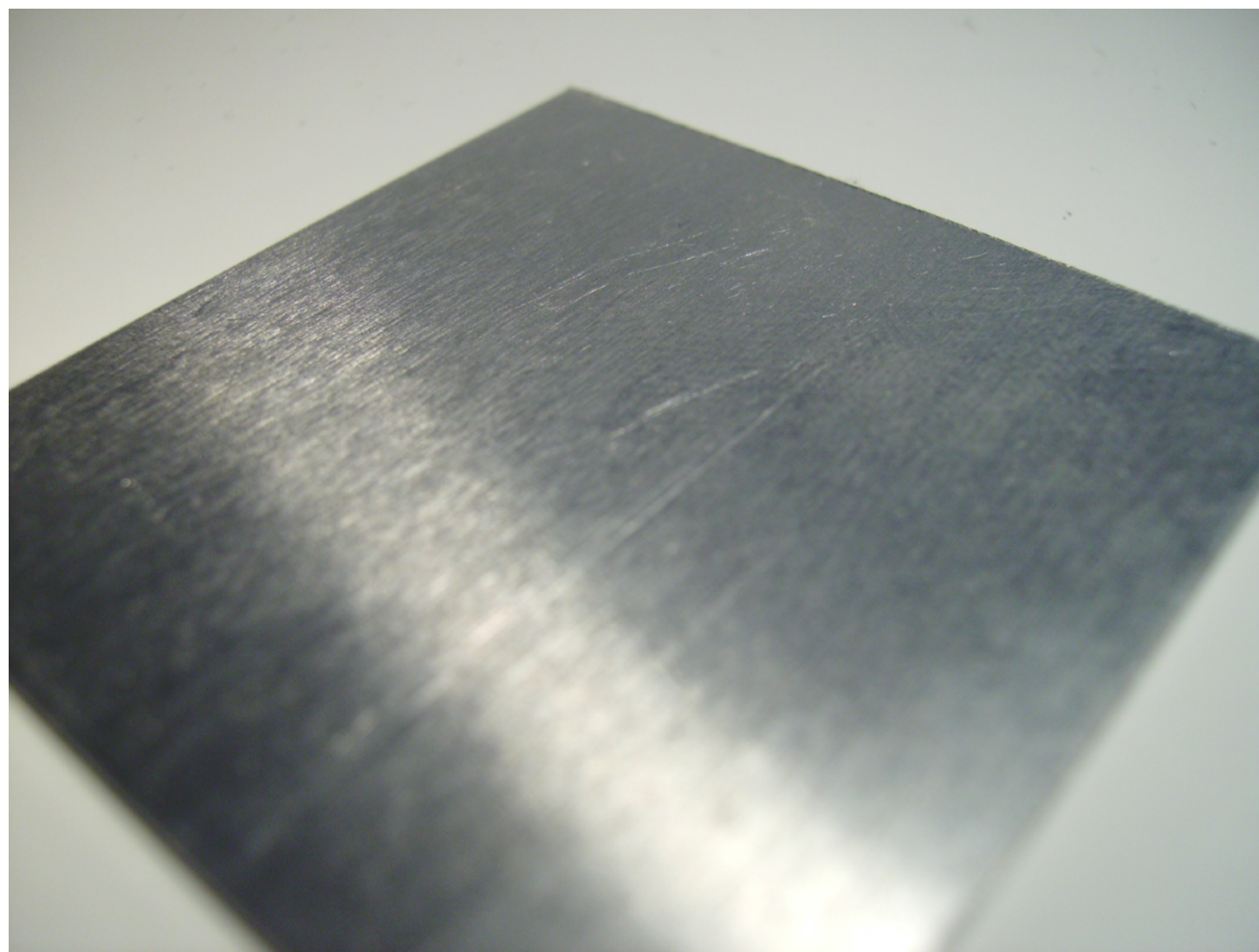
$$f(\omega_i \rightarrow \omega_o) = f(\omega_o \rightarrow \omega_i)$$

Scattered radiance does not obey reciprocity—why?

Properties of BRDFs

3. Isotropic: BRDF is a 3D function

$$f_r((\theta_i, \phi_i) \rightarrow (\theta_o, \phi_o)) \rightarrow f_r(\theta_i, \theta_o, \phi_i - \phi_o)$$



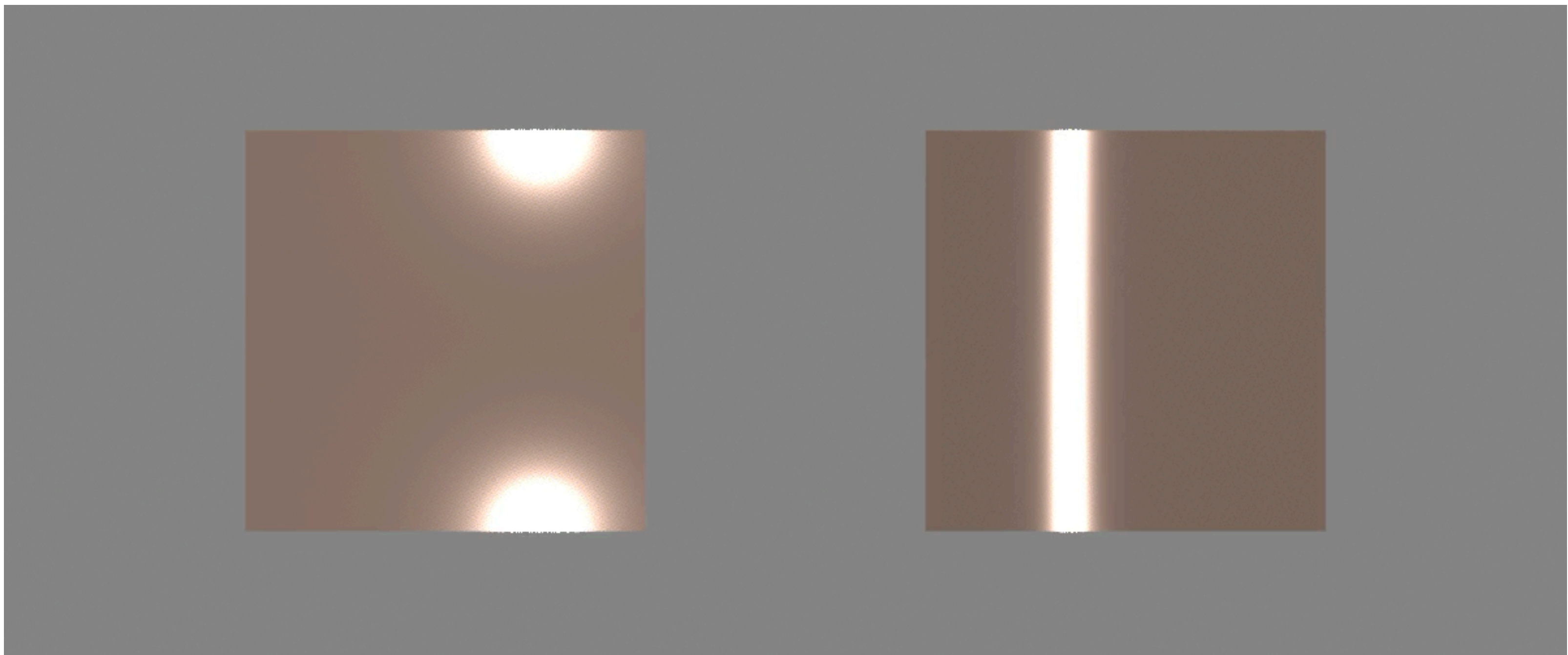
Anisotropic: e.g., brushed metal

(Wikipedia CC-A-SA 3.0)

Properties of BRDFs

3. Isotropic: BRDF is a 3D function

$$f_r((\theta_i, \phi_i) \rightarrow (\theta_o, \phi_o)) \rightarrow f_r(\theta_i, \theta_o, \phi_i - \phi_o)$$

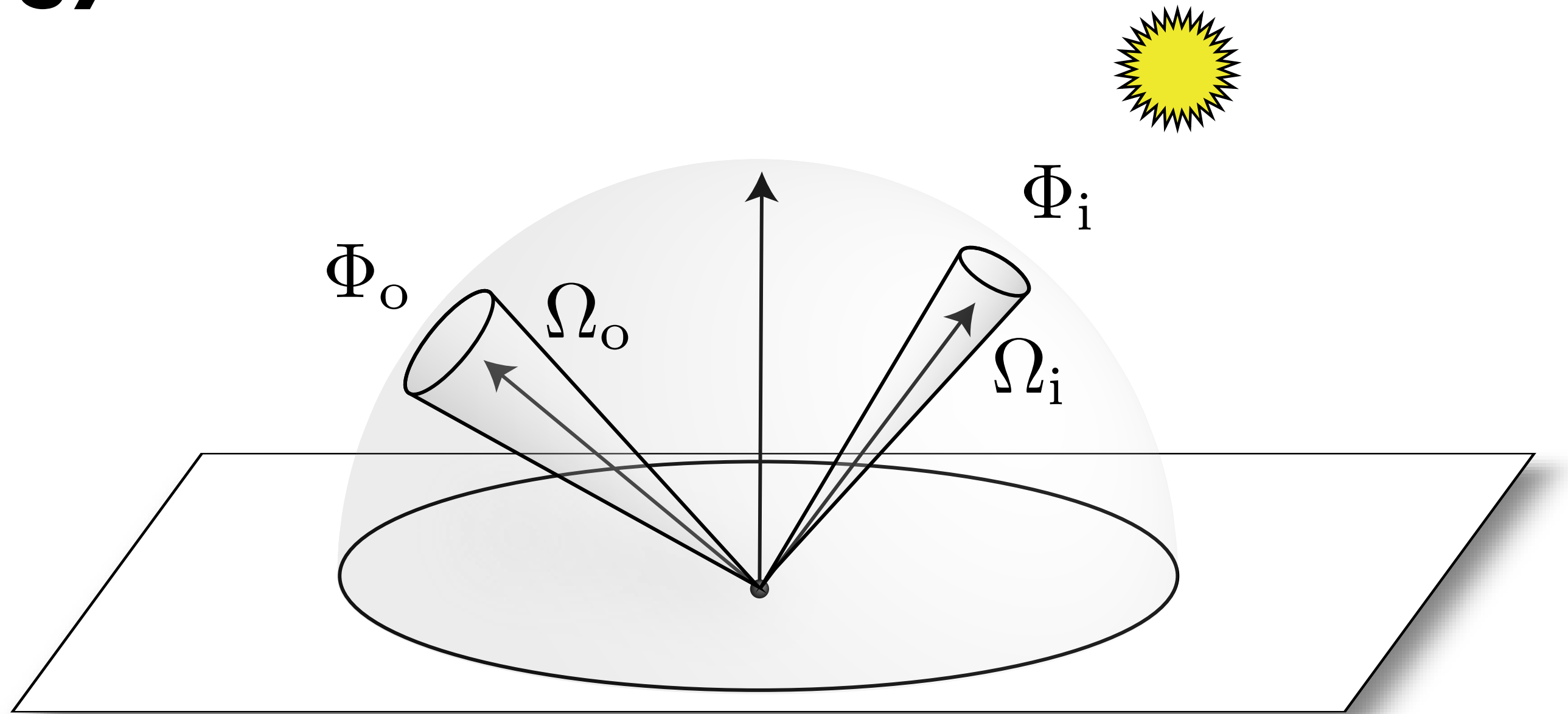


Isotropic

Anisotropic

Properties of BRDFs

4. Energy Conservation



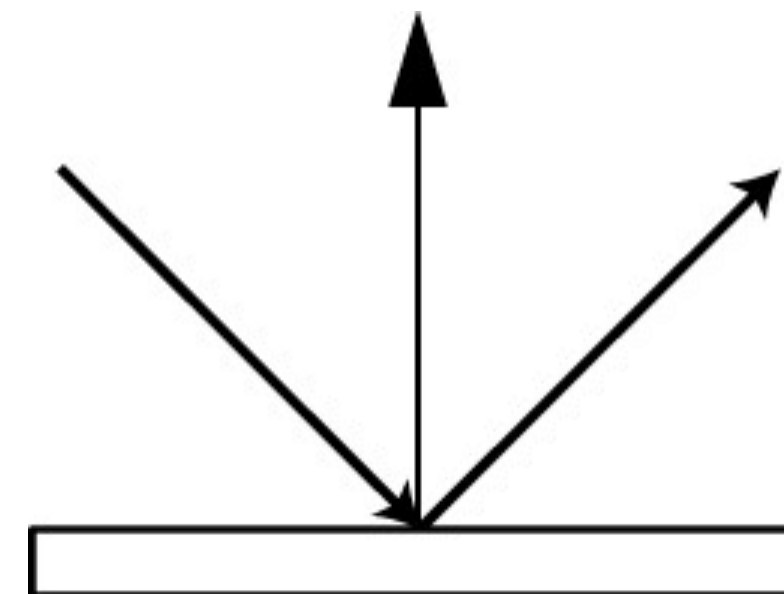
Reflectance $\rho = \frac{\Phi_o}{\Phi_i} = \frac{\int_{\Omega_o} L_o(\omega_o) \cos \theta_o d\omega_o}{\int_{\Omega_i} L_i(\omega_i) \cos \theta_i d\omega_i}$

$$0 \leq \rho \leq 1$$

Types of Reflection Functions

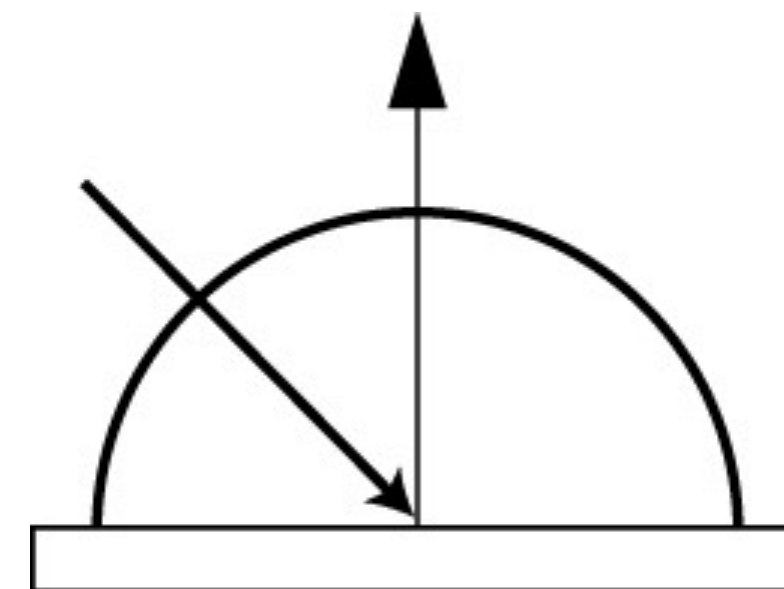
Ideal Specular

- Reflection Law
- Mirror



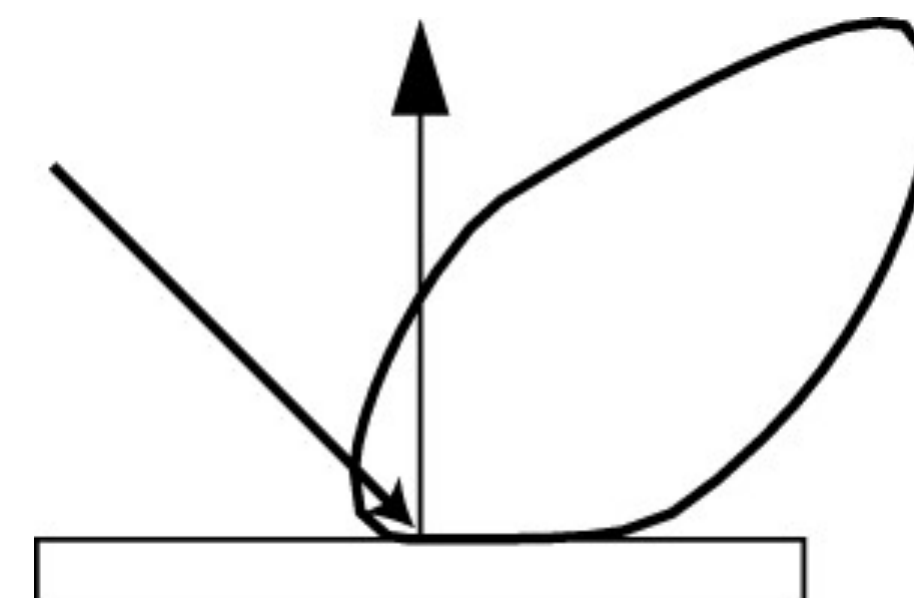
Ideal Diffuse

- Lambert's Law
- Matte

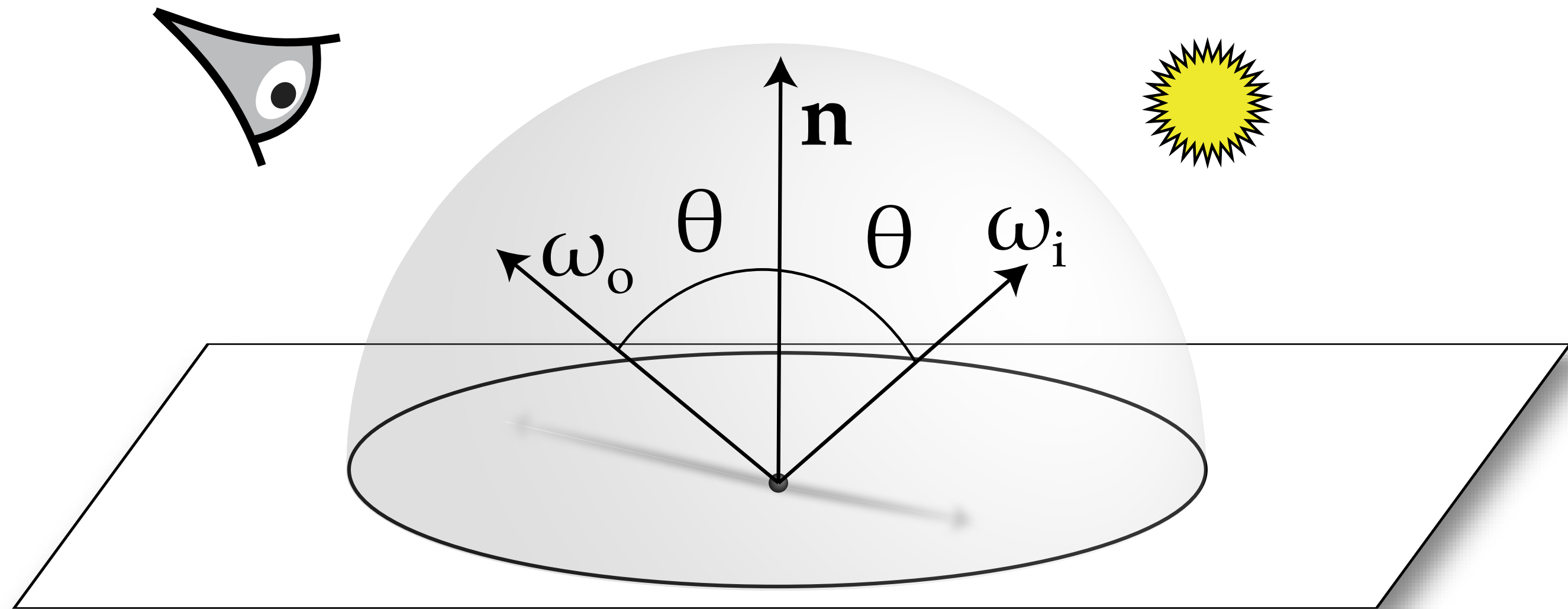


Specular

- Glossy
- Directional diffuse

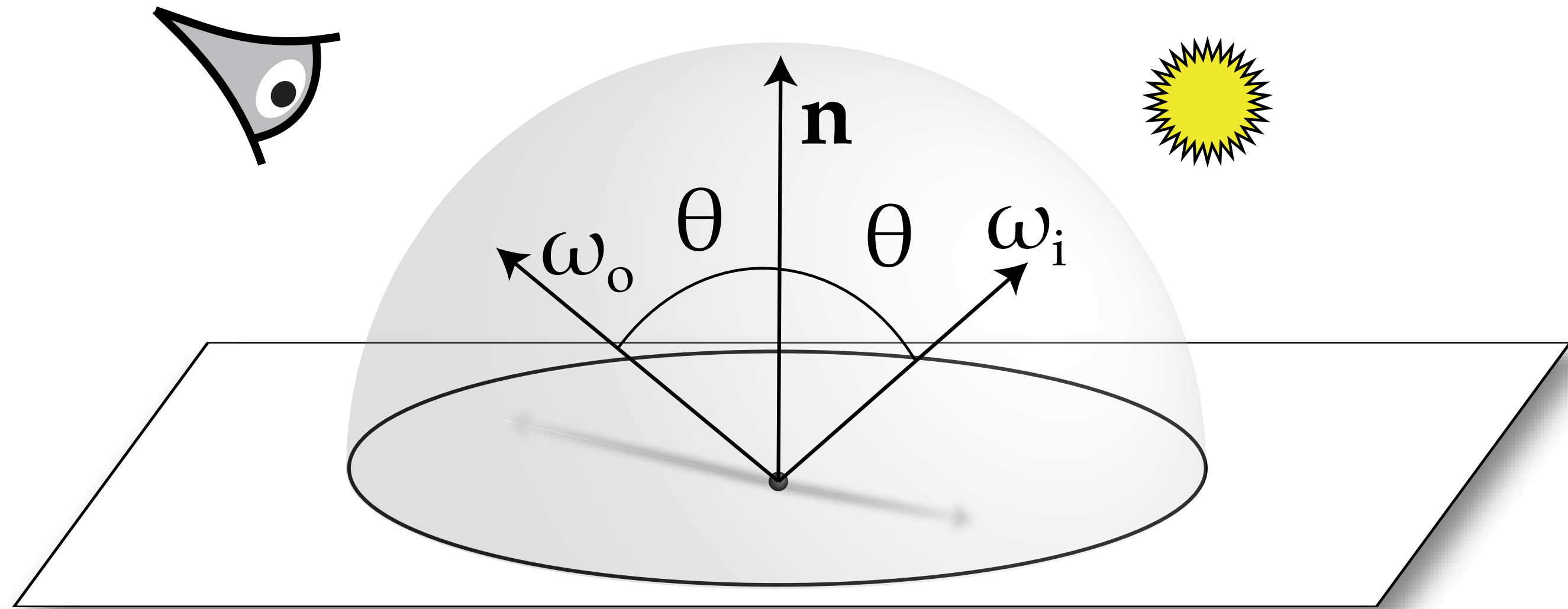


Law of Reflection



$$\omega_i = R(\omega_o, \mathbf{n}) = -\omega_o + 2(\omega_o \cdot \mathbf{n})\mathbf{n}$$

Ideal Reflection BRDF

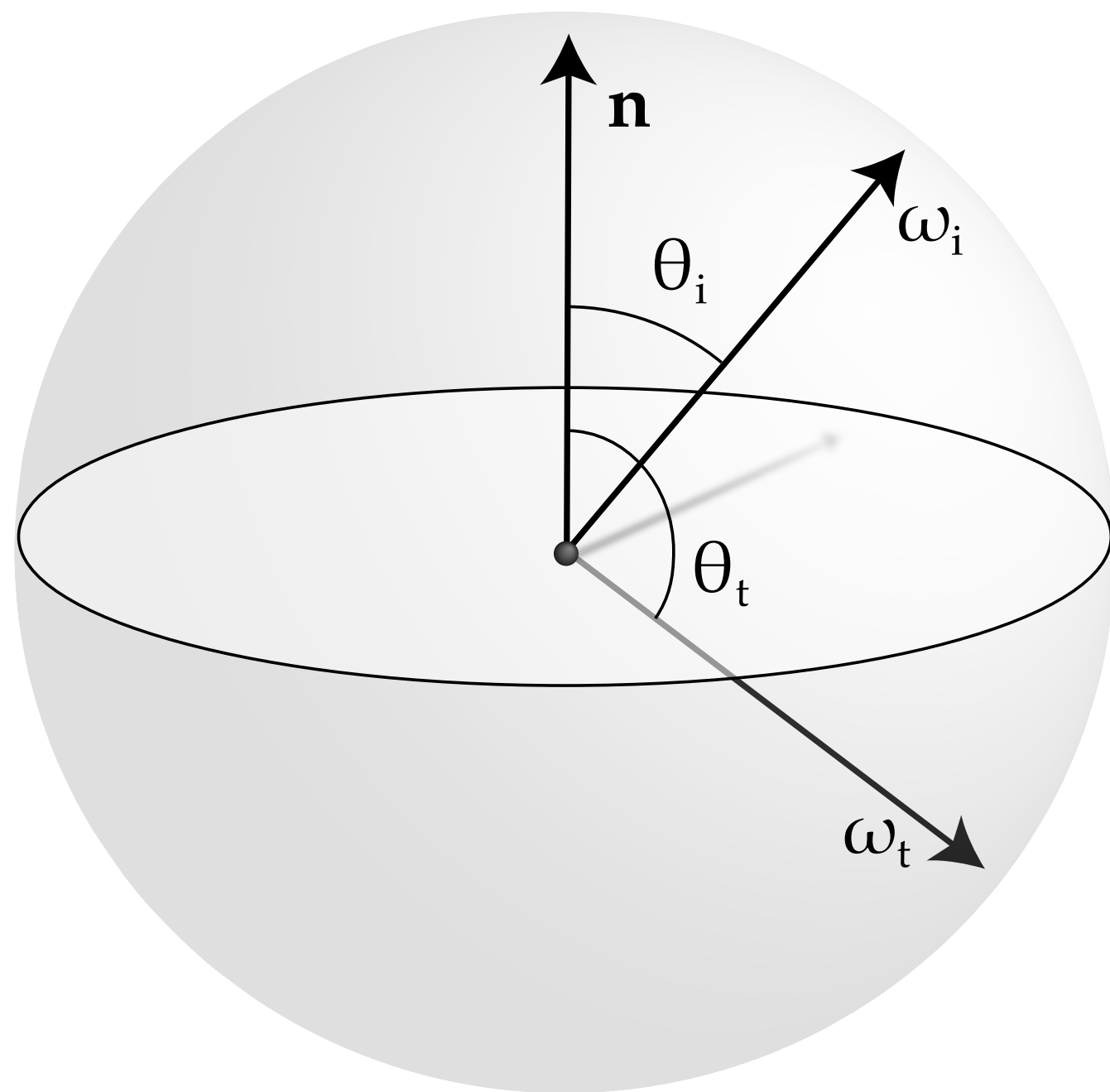


$$f_r(\omega_o \rightarrow \omega_i) = \frac{\delta(\omega_i - R(\omega_o, \mathbf{n}))}{\cos \theta_i}$$

$$\int f_r(\omega_o \rightarrow \omega_i) L_i(\omega_i) \cos \theta_i d\omega_i =$$

$$\int \frac{\delta(\omega_i - R(\omega_o, \mathbf{n}))}{\cos \theta_i} L_i(\omega_i) \cos \theta_i d\omega_i = L_i(\omega_i)$$

Ideal Specular Transmission



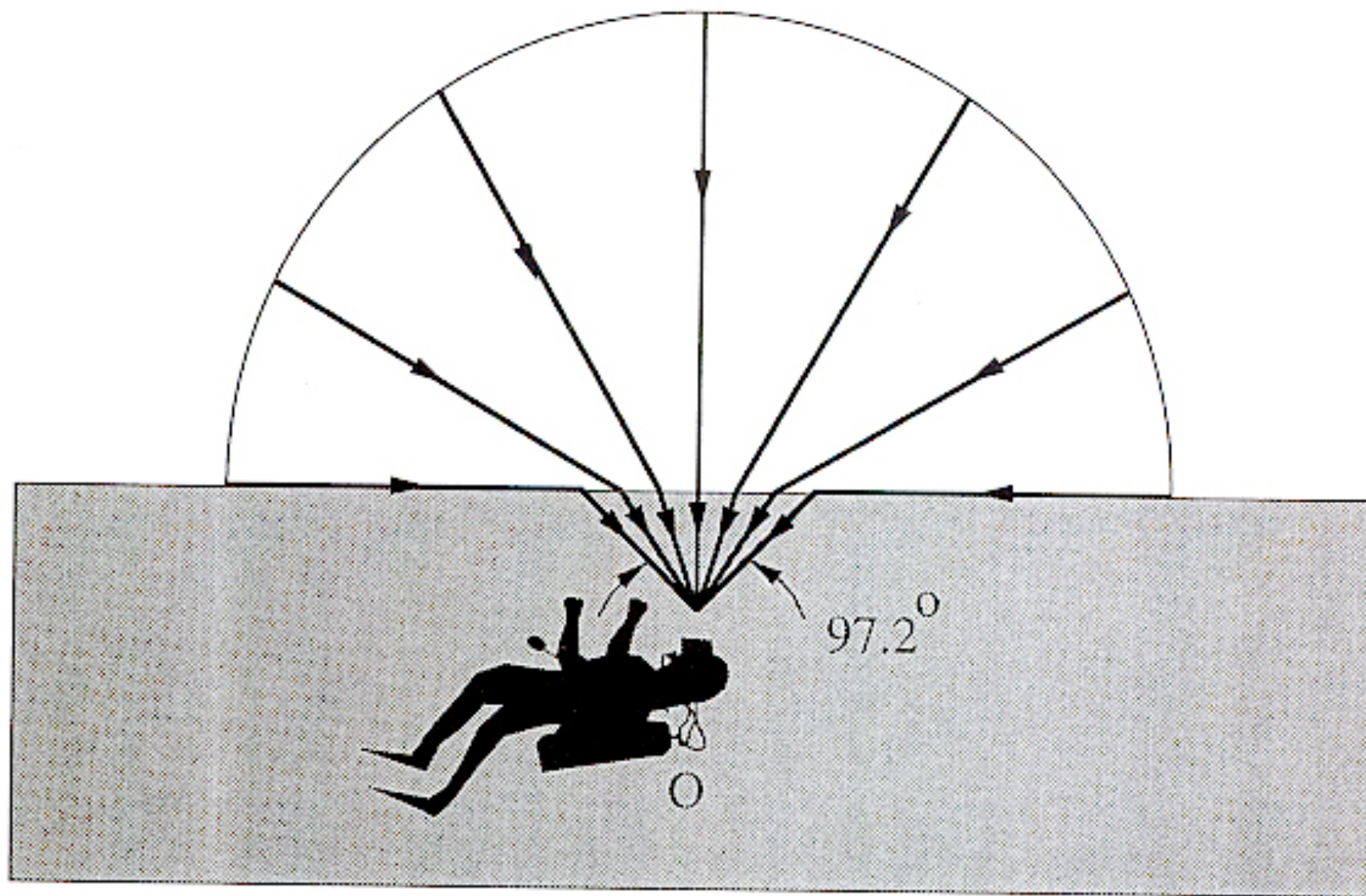
$$\eta = \frac{\eta_i}{\eta_t}$$
$$\omega_t = \frac{-\omega_i}{\eta} + \left(\frac{\cos \theta_i}{\eta} - \cos \theta_t \right) \mathbf{n}$$

Snell's law: $\eta_i \sin \theta_i = \eta_t \sin \theta_t$

Total internal reflection: $\sin \theta_t = \frac{\eta_i}{\eta_t} \sin \theta_i > 1$

Optical Manhole

Total internal reflection

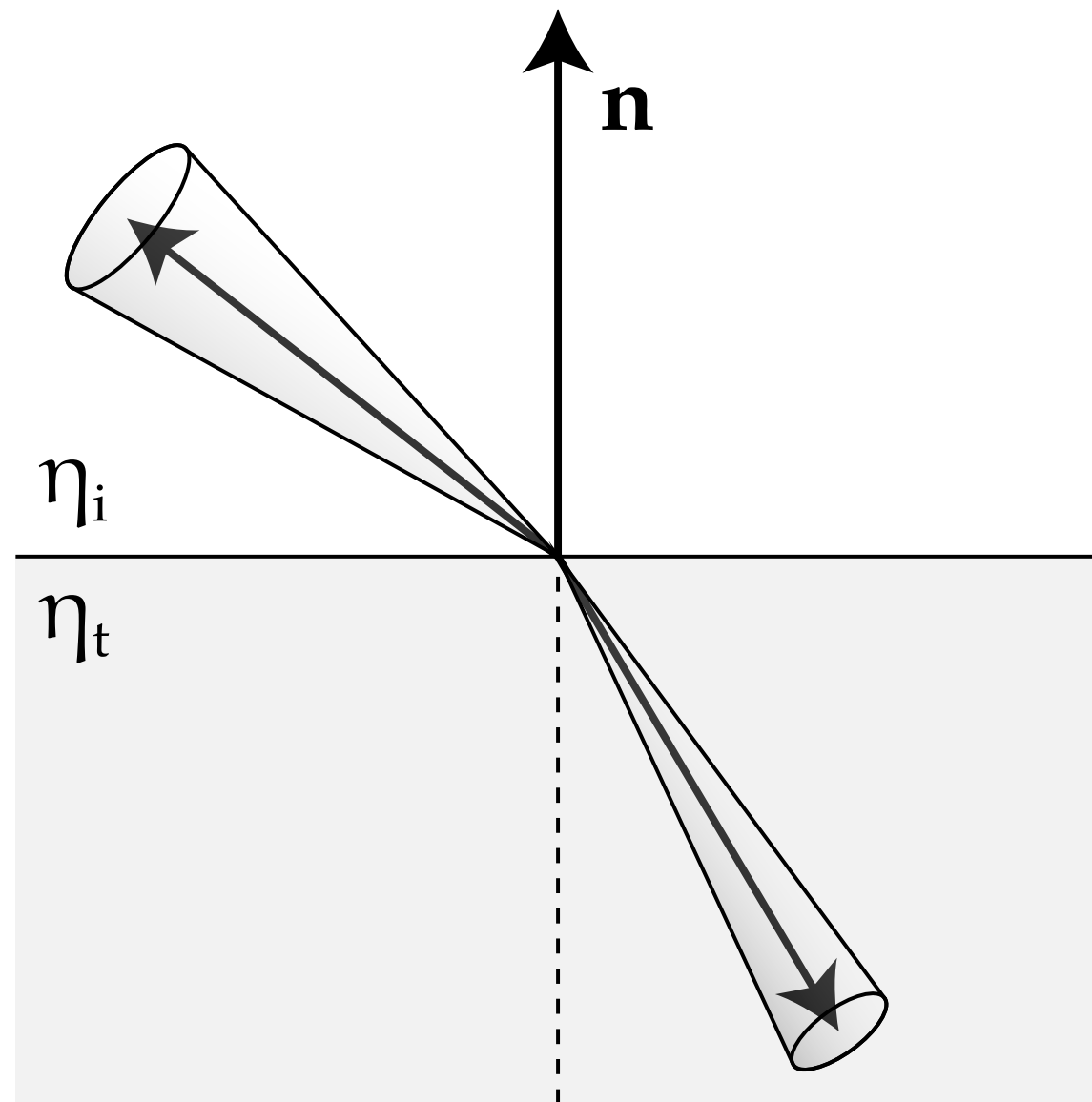


$$n_w = \frac{4}{3}$$



From Livingston and Lynch

Change in Radiance With Refraction

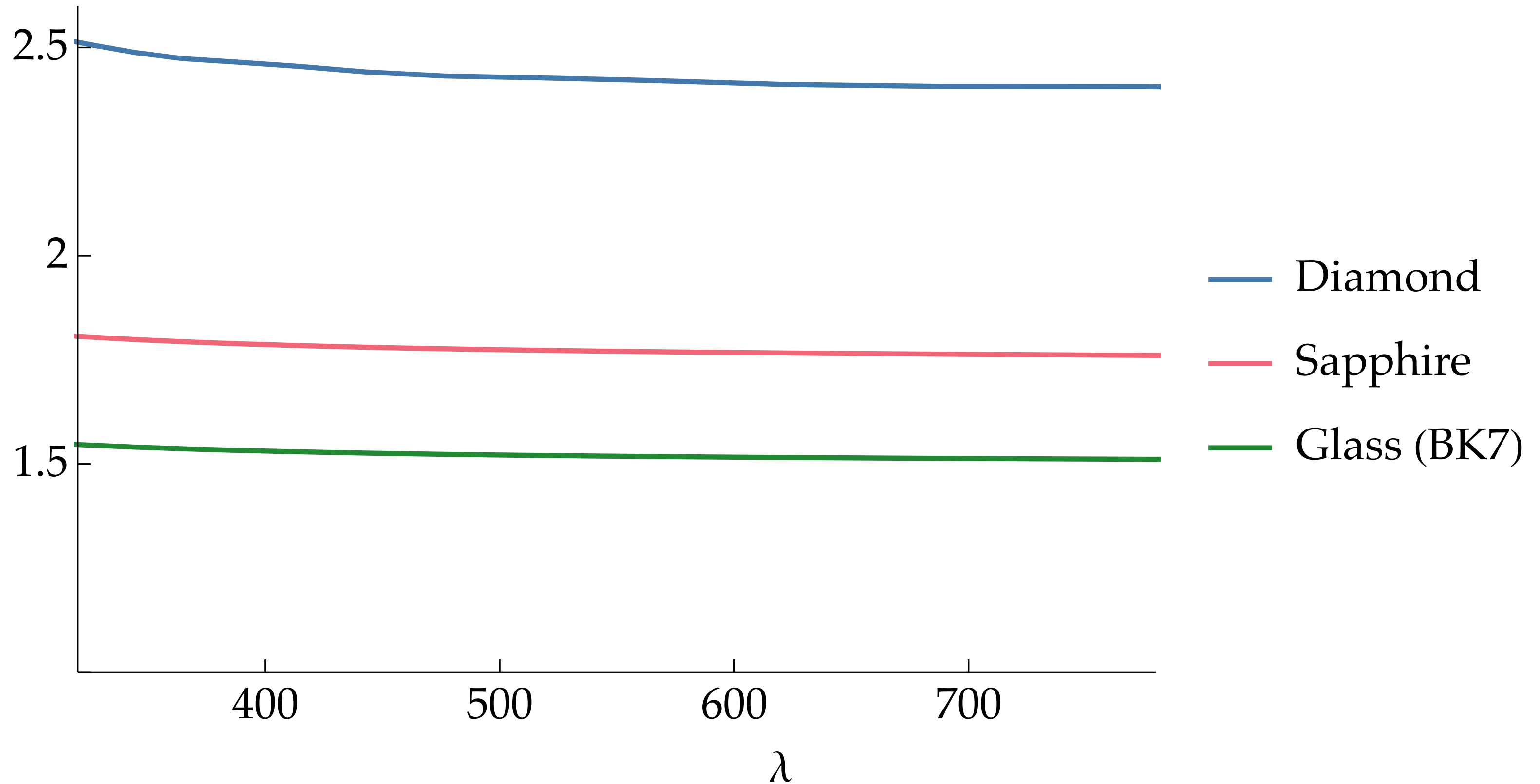


BTDFs are not reciprocal!

$$f_t(\omega_o \rightarrow \omega_i) \neq f_t(\omega_i \rightarrow \omega_o)$$

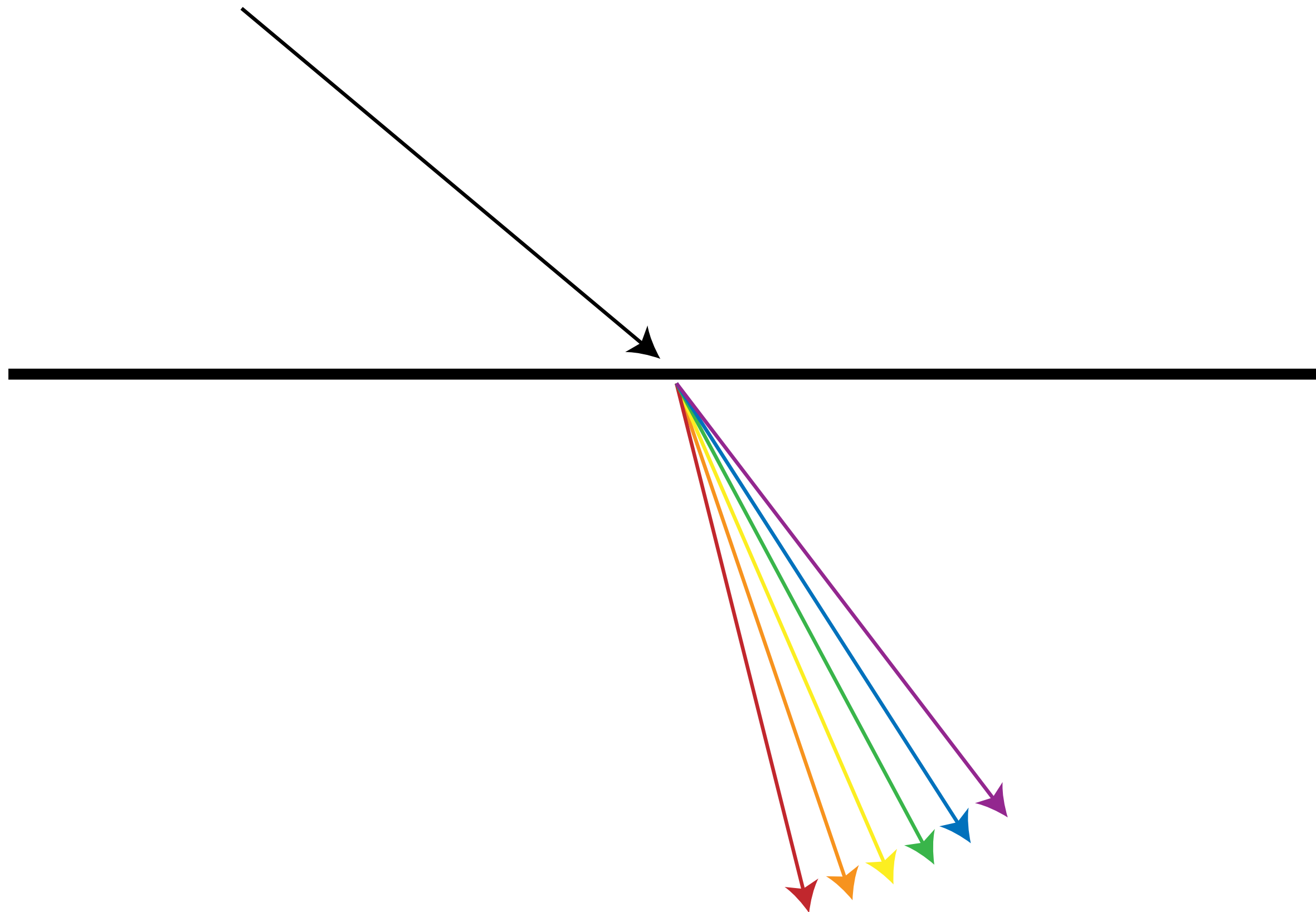
Conservation of basic radiance: $\frac{L_i}{\eta_i^2} = \frac{L_t}{\eta_t^2}$

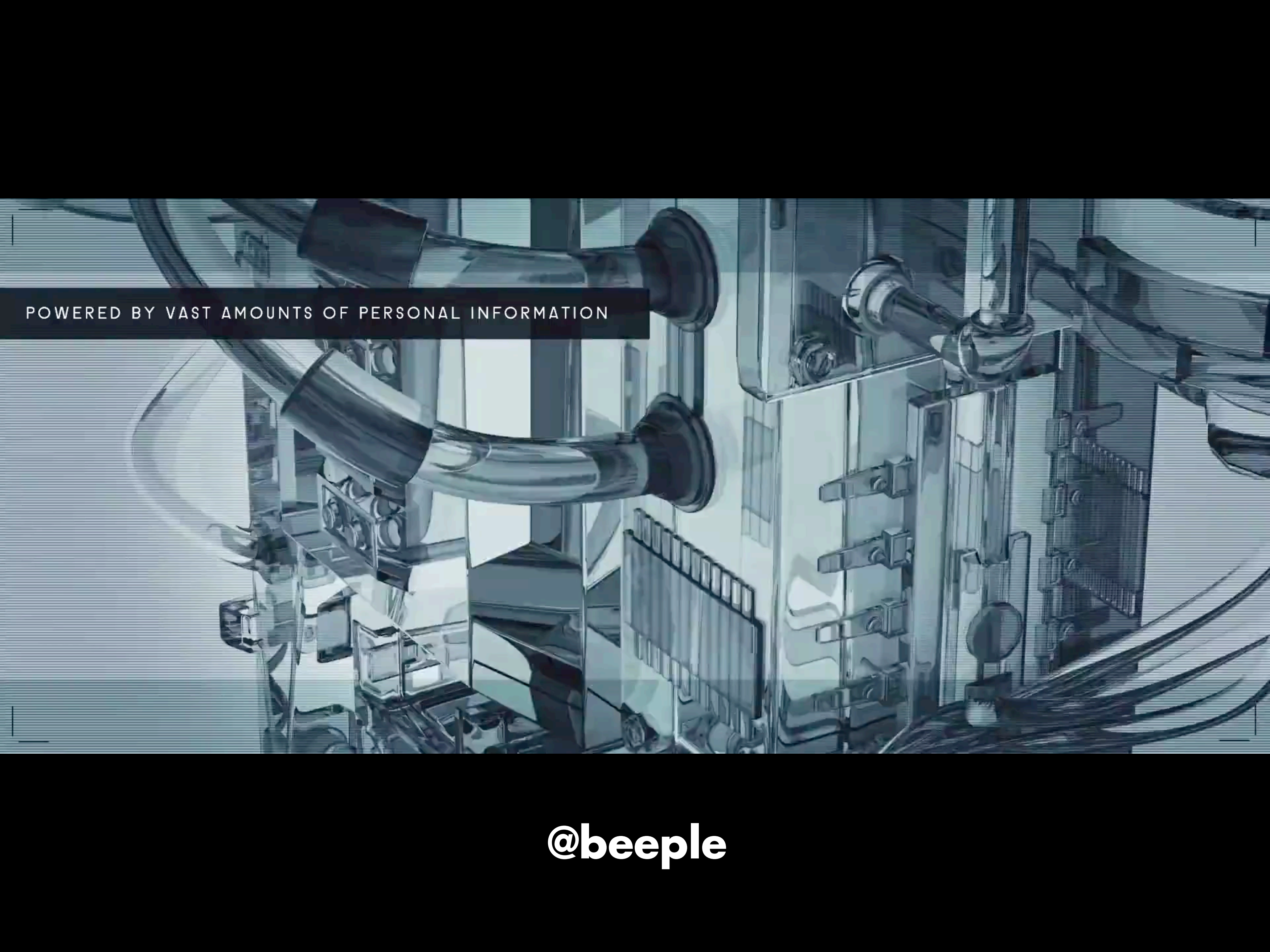
Wavelength-Dependent IOR



<https://refractiveindex.info>

Wavelength-Dependent IOR



A blue-tinted, high-angle view of a modern office interior. The scene shows a grid of desks and glass partitions, with several office chairs visible. The lighting is bright, creating a clean and professional atmosphere. A dark horizontal bar is overlaid on the left side of the image, containing white text.

POWERED BY VAST AMOUNTS OF PERSONAL INFORMATION

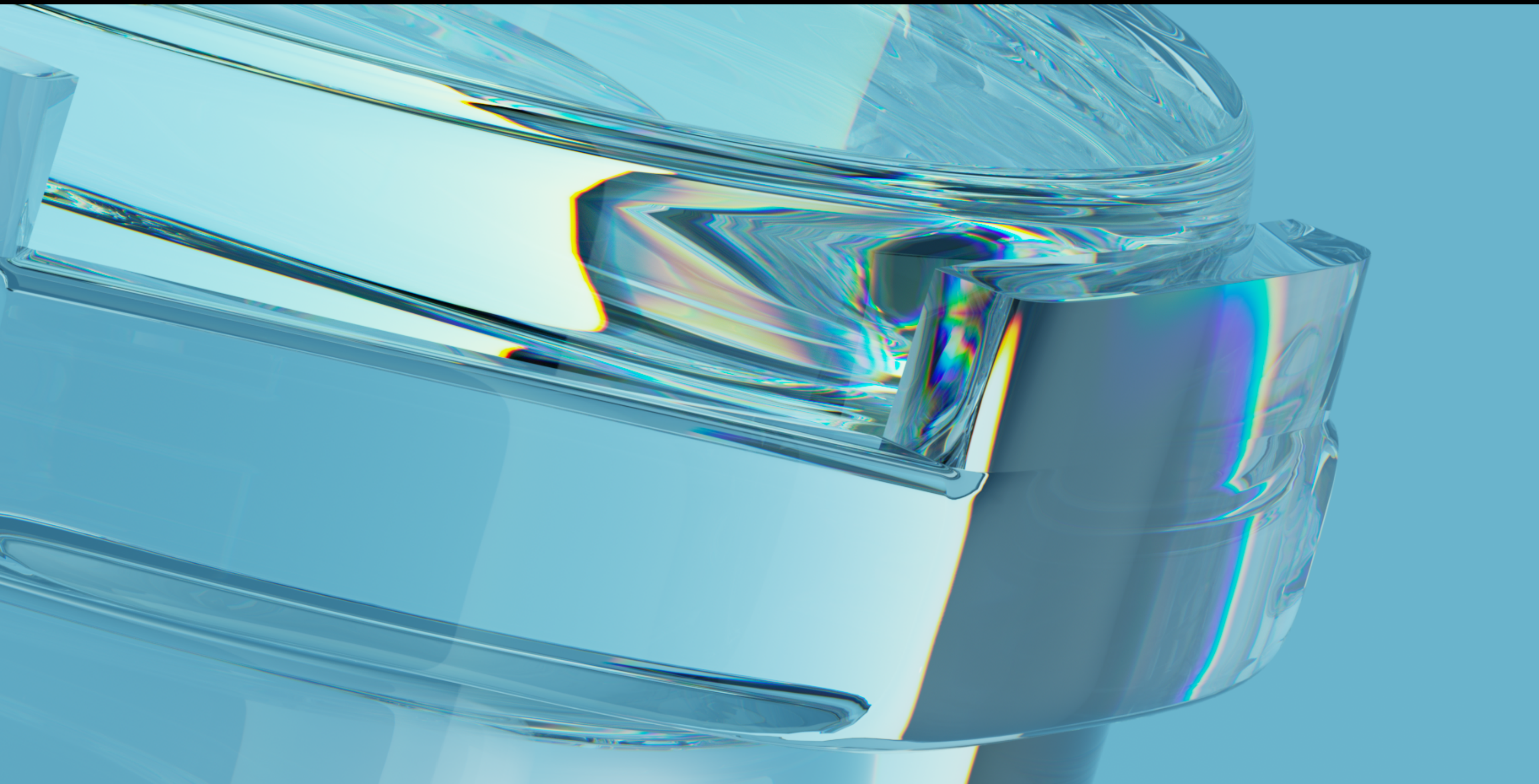
@beeple

Fixed Index of Refraction



@beepie

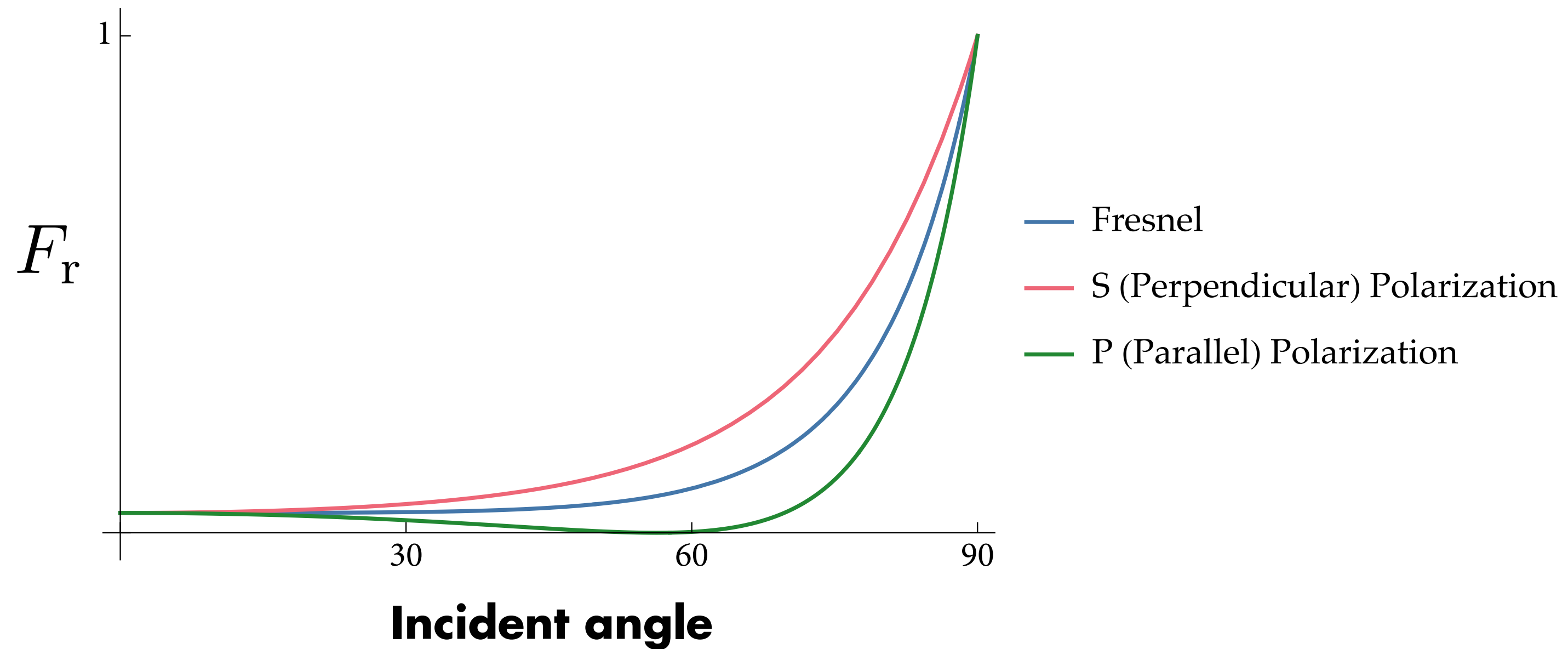
Wavelength-Dependent IOR



@beepie

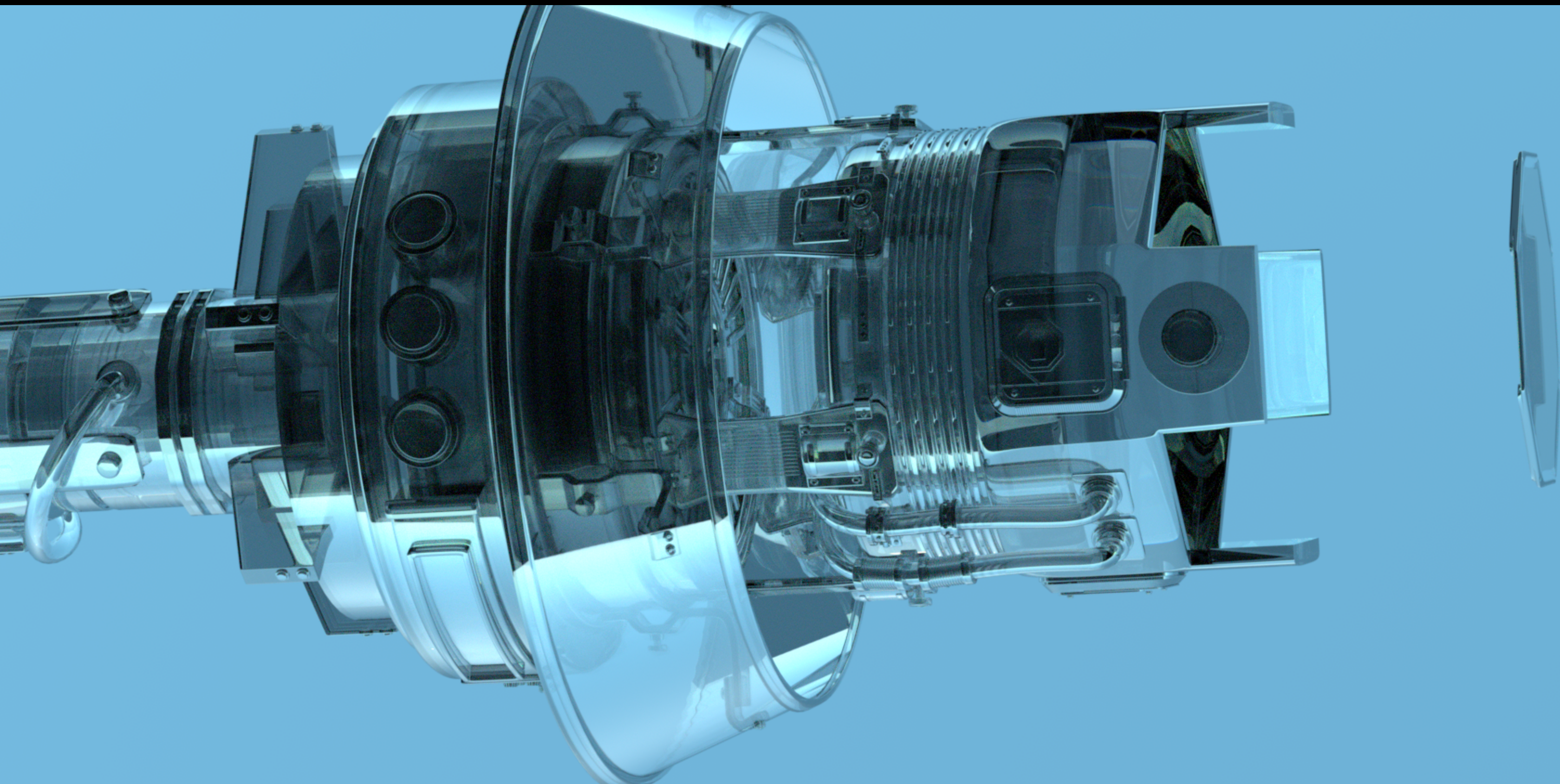
Fresnel Reflectance

Dielectric (Glass $\eta = 1.5$)



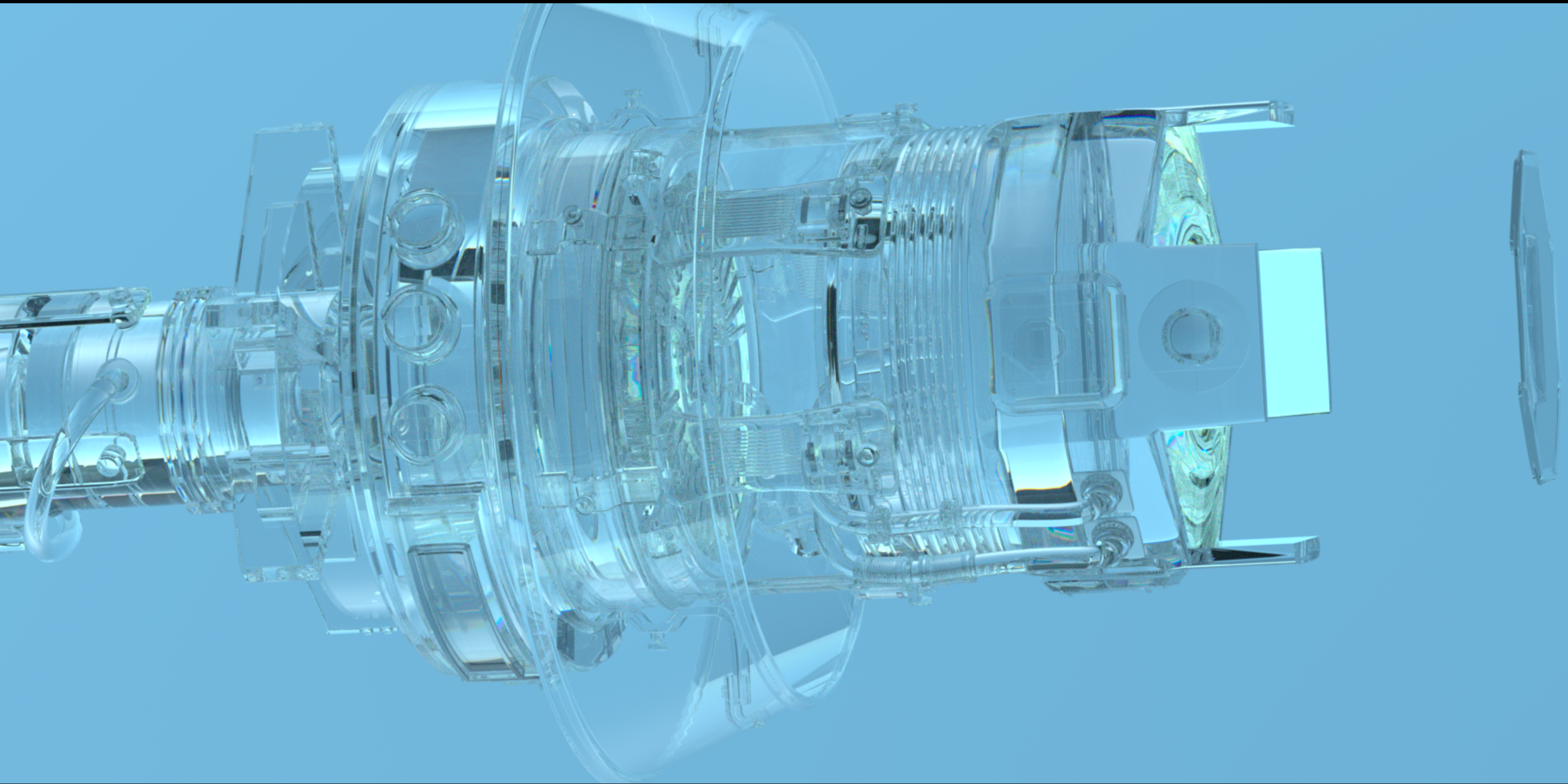
Transmission: $1 - F_r$

Reflect 0.5, Transmit 0.5



@beepie

Fresnel Reflection and Transmission



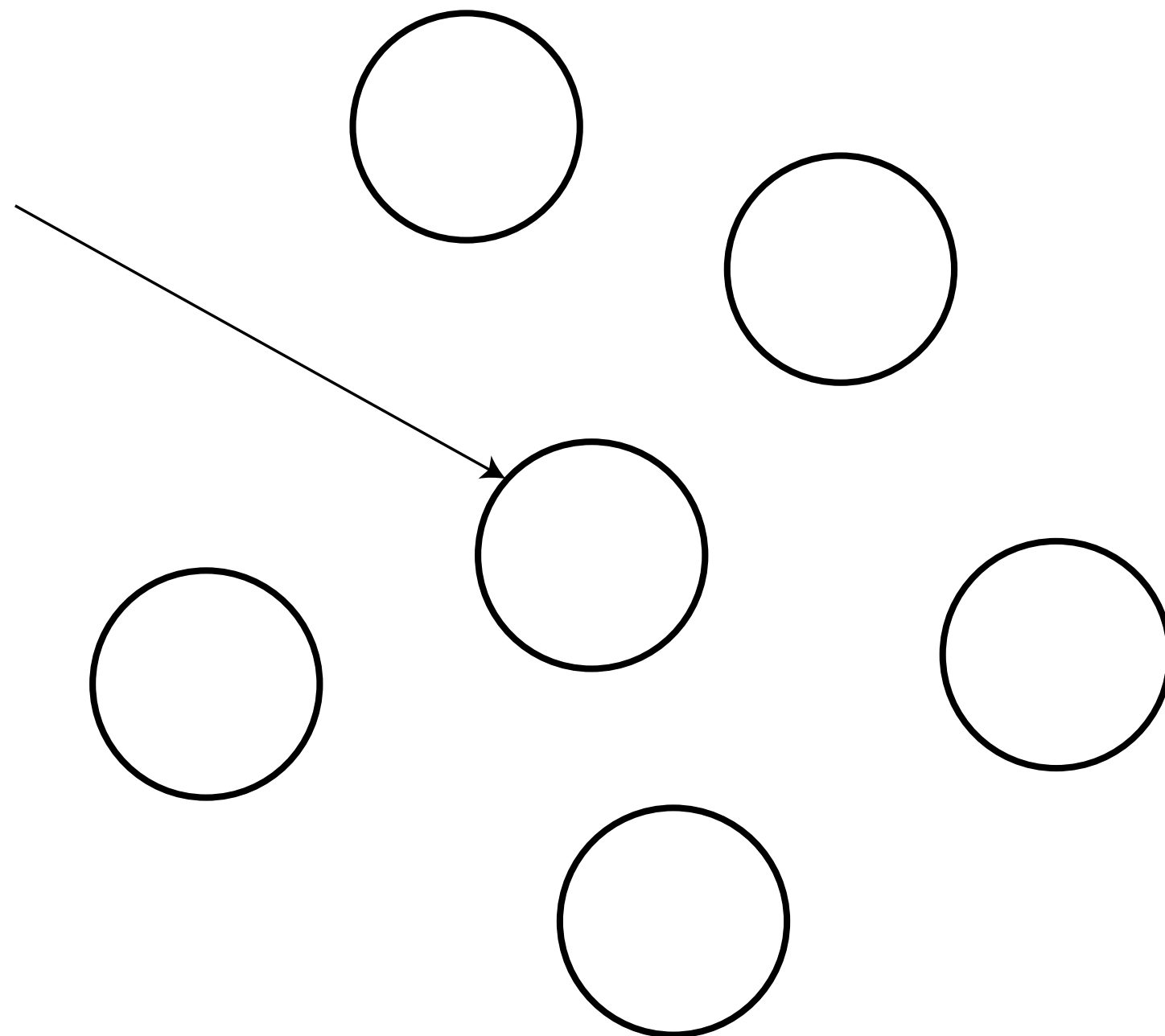
@beepie

Sampling Reflection + Transmission

$$\begin{aligned} L_o(\mathbf{p}, \omega) &= \int_{\mathcal{S}^2} f(\mathbf{p}, \omega_i \rightarrow \omega_o) L_i(\mathbf{p}, \omega_i) \cos \theta_i d\omega_i \\ &= \int_{\mathcal{S}^2} \left(F_r \frac{\delta(\omega_i - R(\omega_o, \mathbf{n}))}{\cos \theta_i} + (1 - F_r) \frac{\delta(\omega_i - T(\omega_o, \mathbf{n}))}{\cos \theta_i} \right) L_i(\mathbf{p}, \omega_i) \cos \theta_i d\omega_i \\ &= F_r L_i(\mathbf{p}, R(\omega_o, \mathbf{n})) + (1 - F_r) L_i(\mathbf{p}, T(\omega_o, \mathbf{n})) \end{aligned}$$

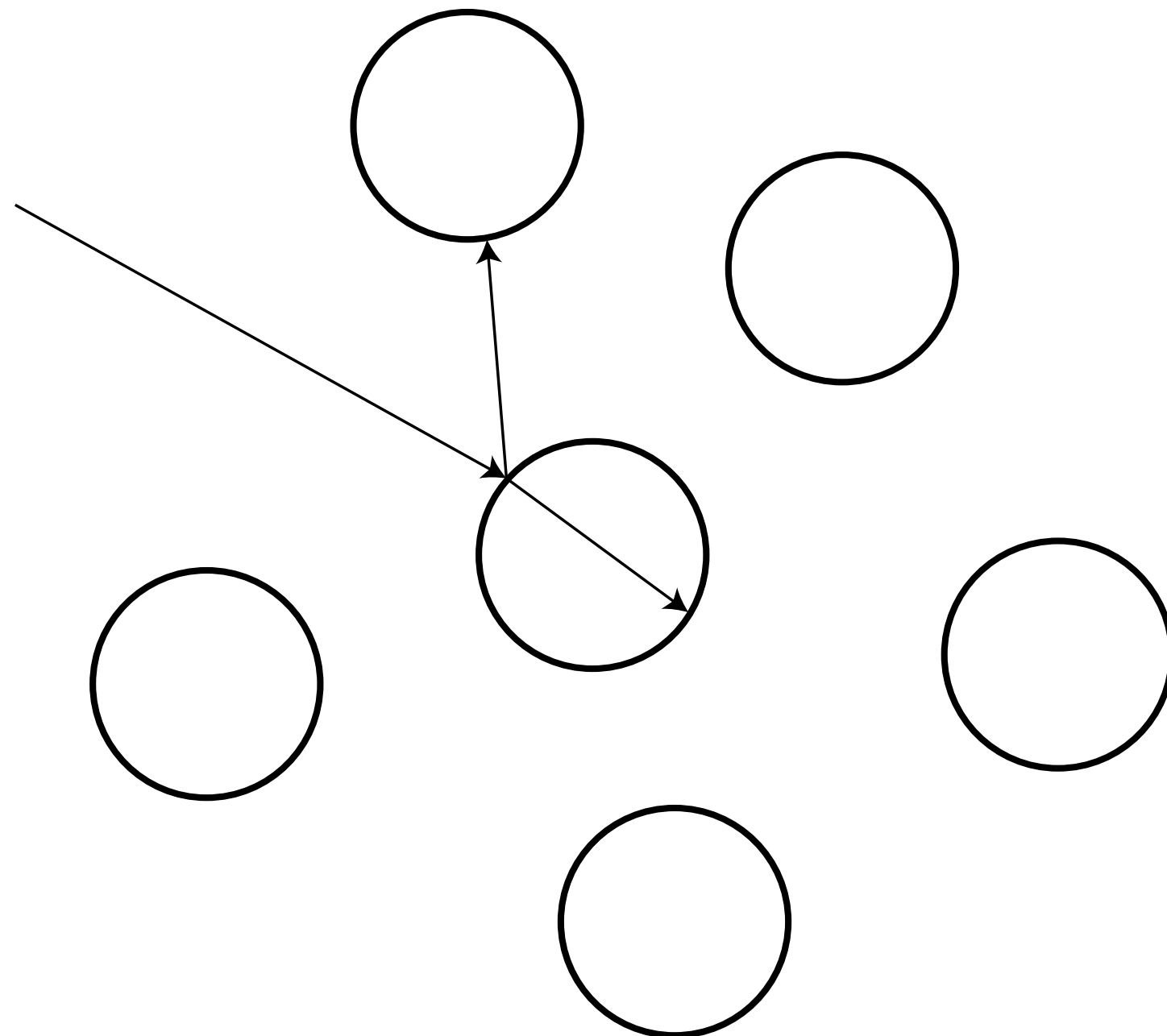
Sampling Reflection + Transmission

$$L_o(p, \omega) = F_r L_i(p, R(\omega_o, \mathbf{n})) + (1 - F_r) L_i(p, T(\omega_o, \mathbf{n}))$$



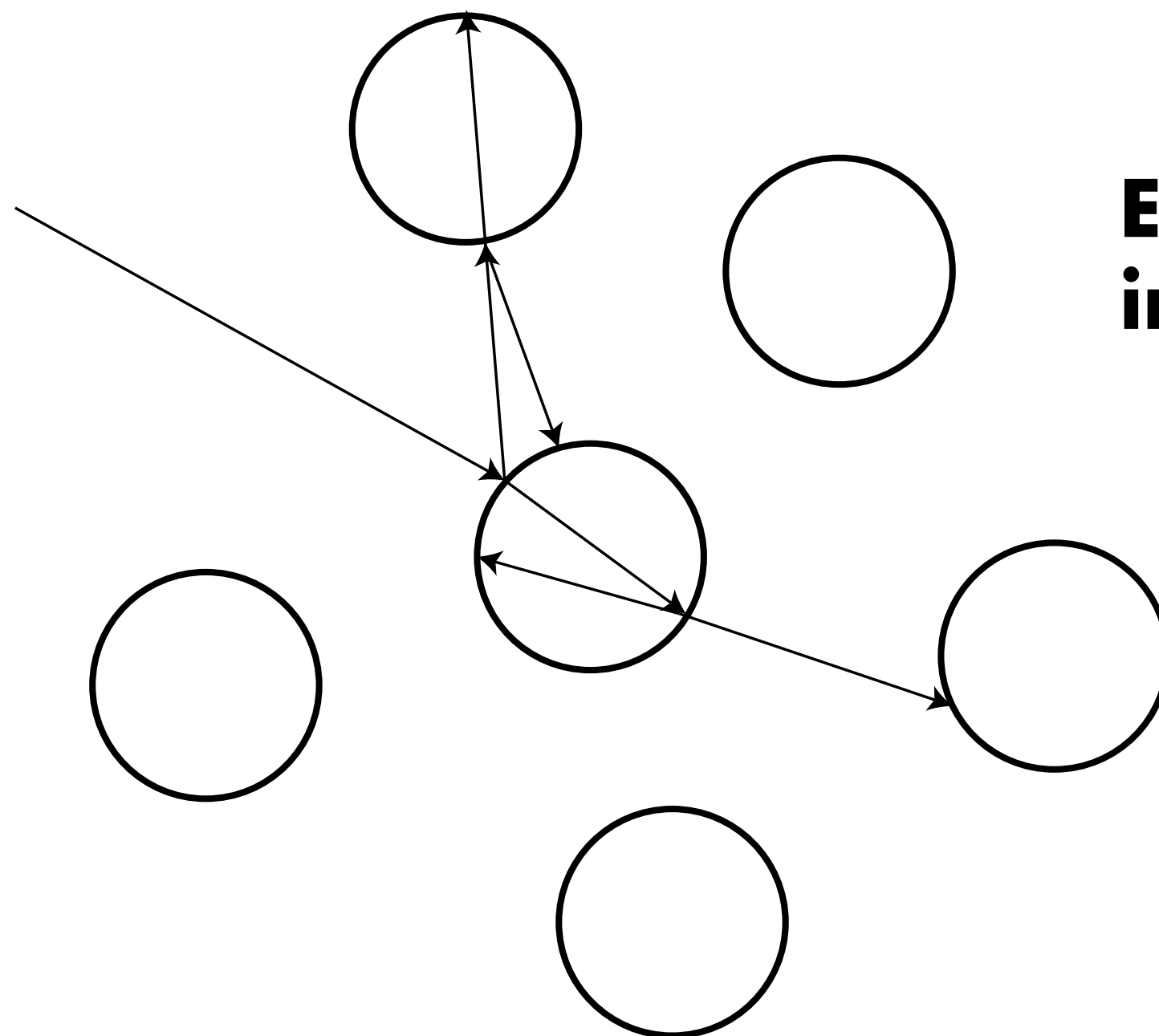
Sampling Reflection + Transmission

$$L_o(p, \omega) = F_r L_i(p, R(\omega_o, \mathbf{n})) + (1 - F_r) L_i(p, T(\omega_o, \mathbf{n}))$$



Sampling Reflection + Transmission

$$L_o(p, \omega) = F_r L_i(p, R(\omega_o, n)) + (1 - F_r) L_i(p, T(\omega_o, n))$$



**Exponential growth
in number of rays!**

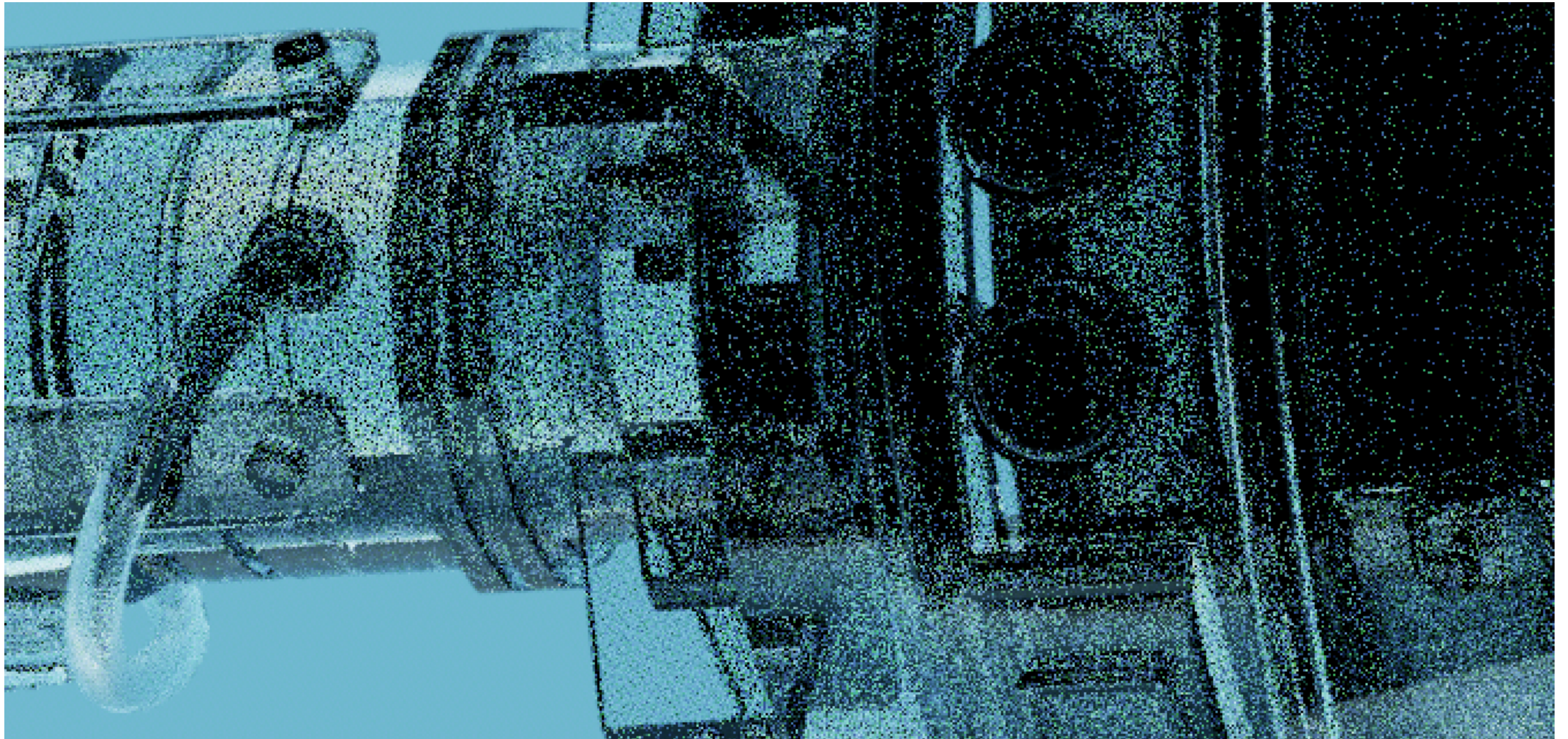
Sampling Reflection + Transmission

Monte Carlo: evaluate a single term using probability p_r

$$L_o(p, \omega) = F_r L_i(p, R(\omega_o, n)) + (1 - F_r) L_i(p, T(\omega_o, n))$$

$$\approx \begin{cases} \frac{F_r L_i(p, R(\omega_o, n))}{p_r}, & \text{with probability } p_r \\ \frac{(1 - F_r) L_i(p, T(\omega_o, n))}{1 - p_r}, & \text{otherwise} \end{cases}$$

Sampling Reflection + Transmission



$$p_r = \frac{1}{2}$$

Sampling Reflection + Transmission

Monte Carlo: evaluate a single term using probability p_r

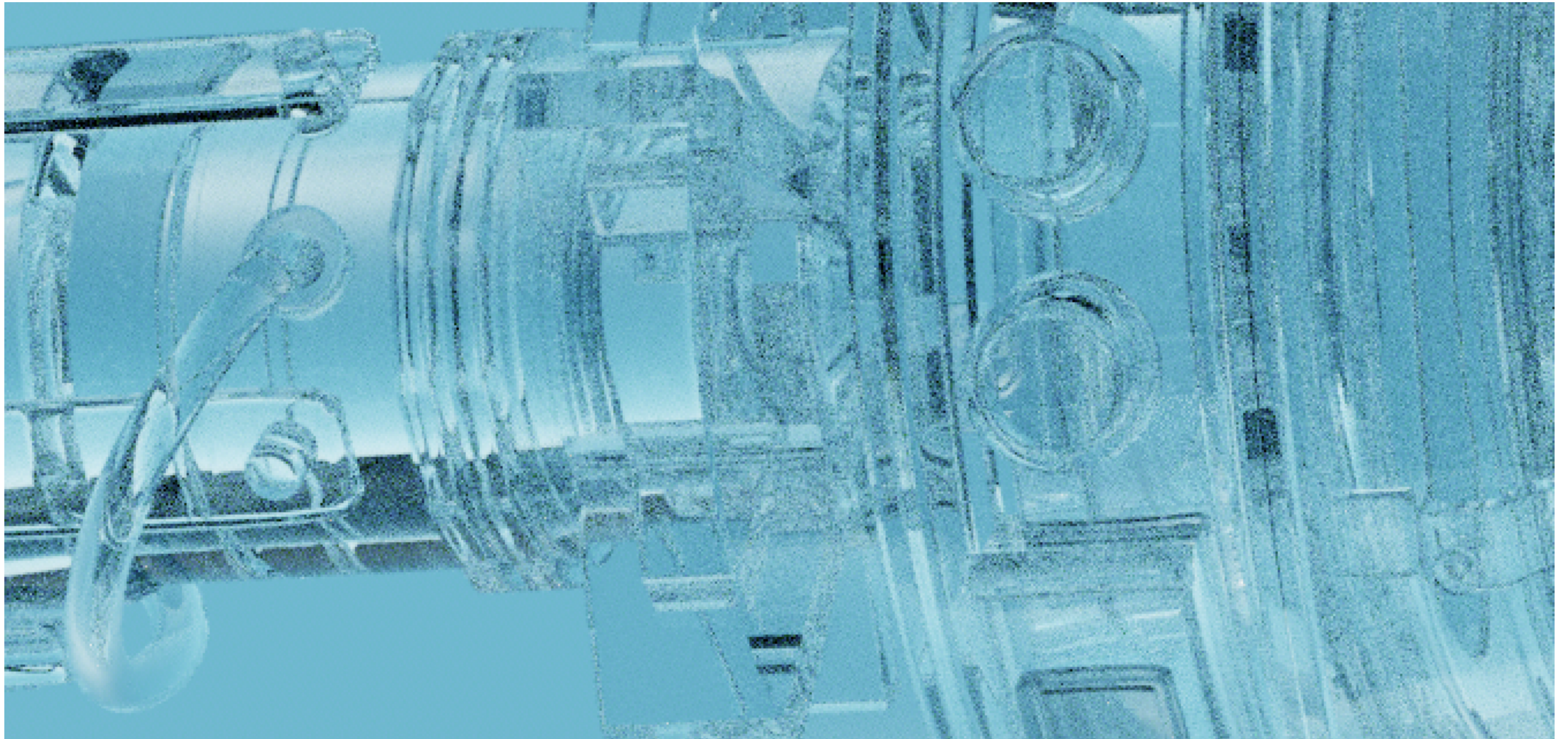
$$L_o(p, \omega) = F_r L_i(p, R(\omega_o, n)) + (1 - F_r) L_i(p, T(\omega_o, n))$$

$$\approx \begin{cases} \frac{F_r L_i(p, R(\omega_o, n))}{p_r}, & \text{with probability } p_r \\ \frac{(1 - F_r) L_i(p, T(\omega_o, n))}{1 - p_r}, & \text{otherwise} \end{cases}$$

Best approach: $p_r = F_r$

$$L_o(p, \omega) \approx \begin{cases} L_i(p, R(\omega_o, n)), & \text{with probability } F_r \\ L_i(p, T(\omega_o, n)), & \text{otherwise} \end{cases}$$

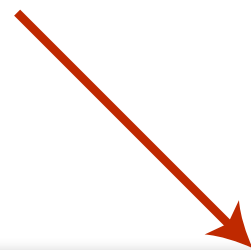
Sampling Reflection + Transmission



$$p_r = F_r$$

Thin Dielectric BSDF

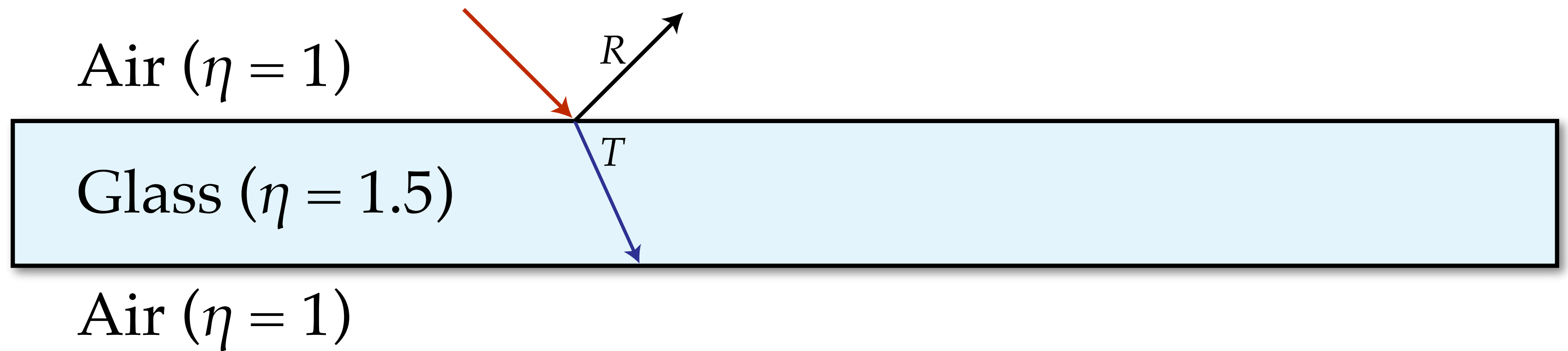
Air ($\eta = 1$)



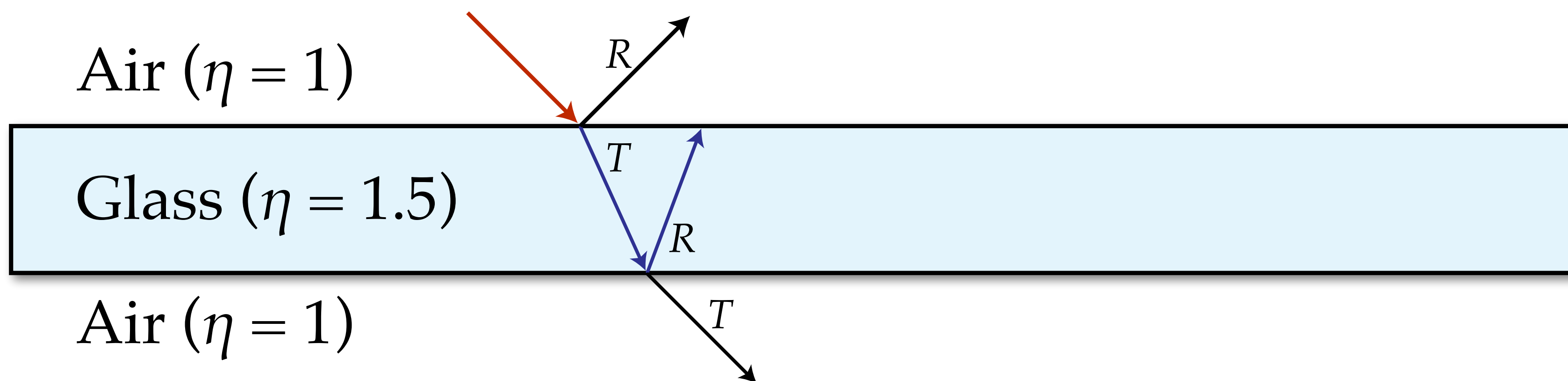
Glass ($\eta = 1.5$)

Air ($\eta = 1$)

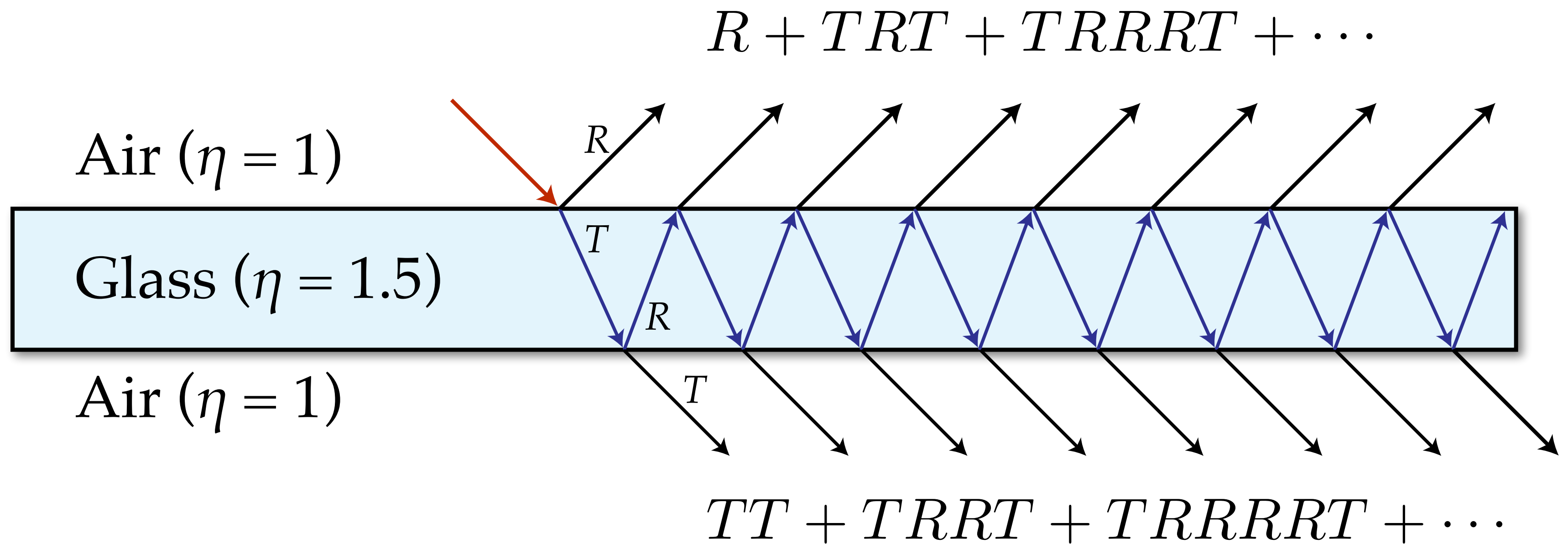
Thin Dielectric BSDF



Thin Dielectric BSDF

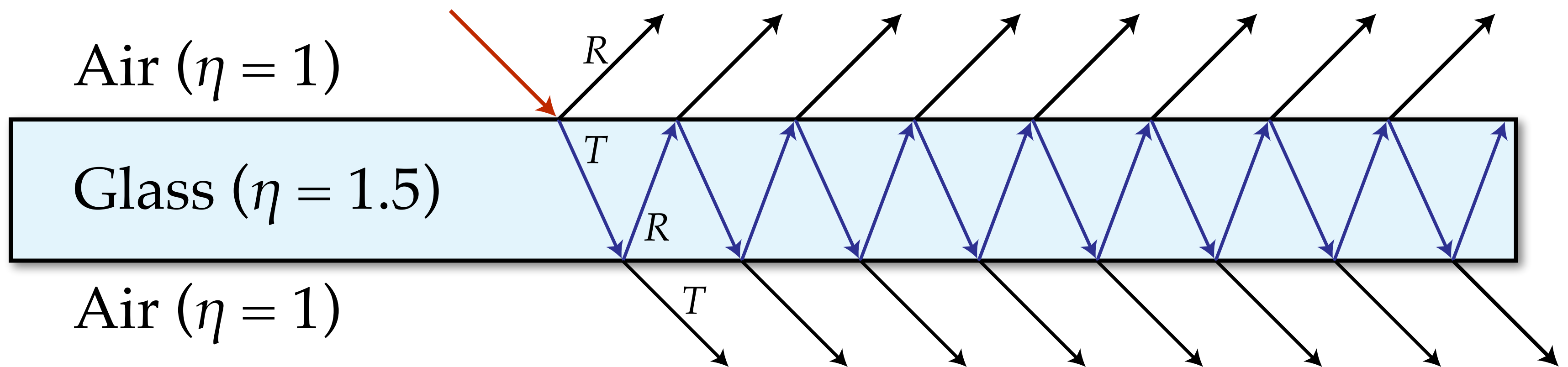


Thin Dielectric BSDF



Thin Dielectric BSDF

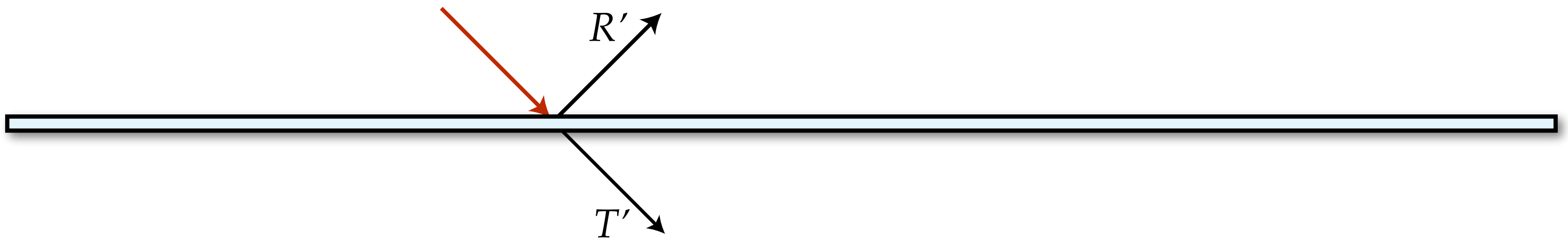
$$R' = R + TRT + TRRRT + \dots = R + \frac{T^2 R}{1 - R^2}$$



$$T' = TT + TRRT + TRRRTT + \dots = 1 - R'$$

Thin Dielectric BSDF

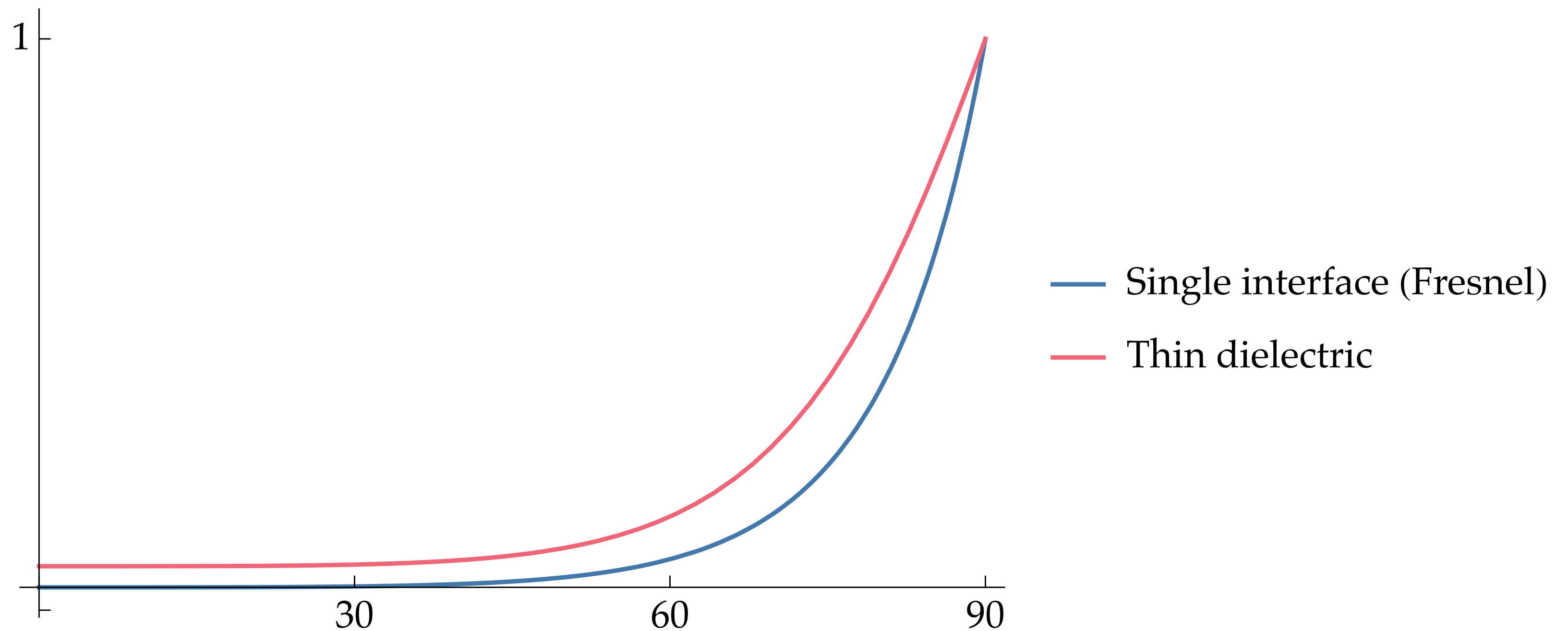
$$R' = R + TRT + TRRRT + \dots = R + \frac{T^2 R}{1 - R^2}$$



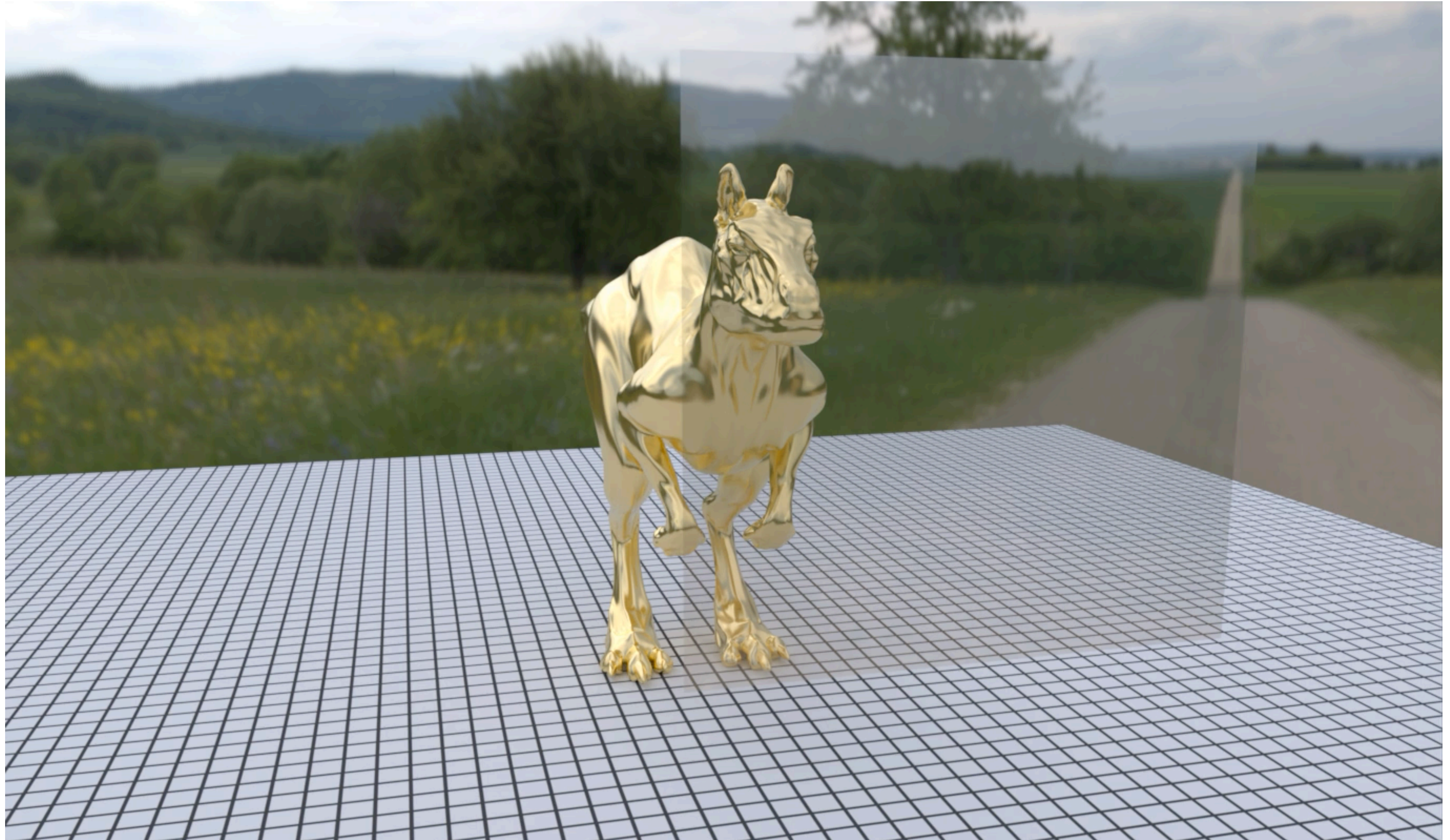
$$T' = TT + TRRT + TRRRRT + \dots = 1 - R'$$

[Stokes 1860] On the intensity of the light reflected from or transmitted through a pile of plates.

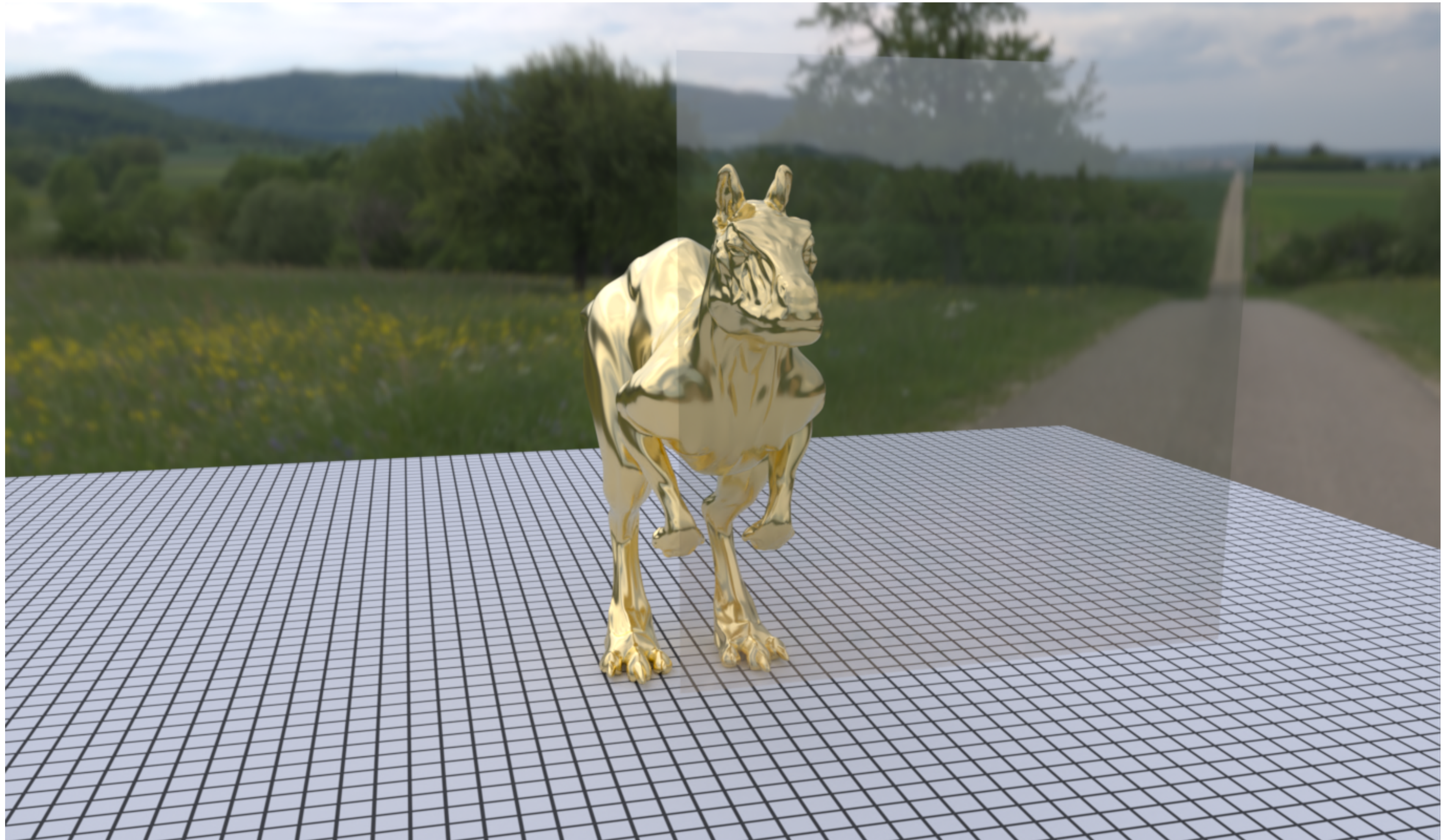
Thin Dielectric Reflectance



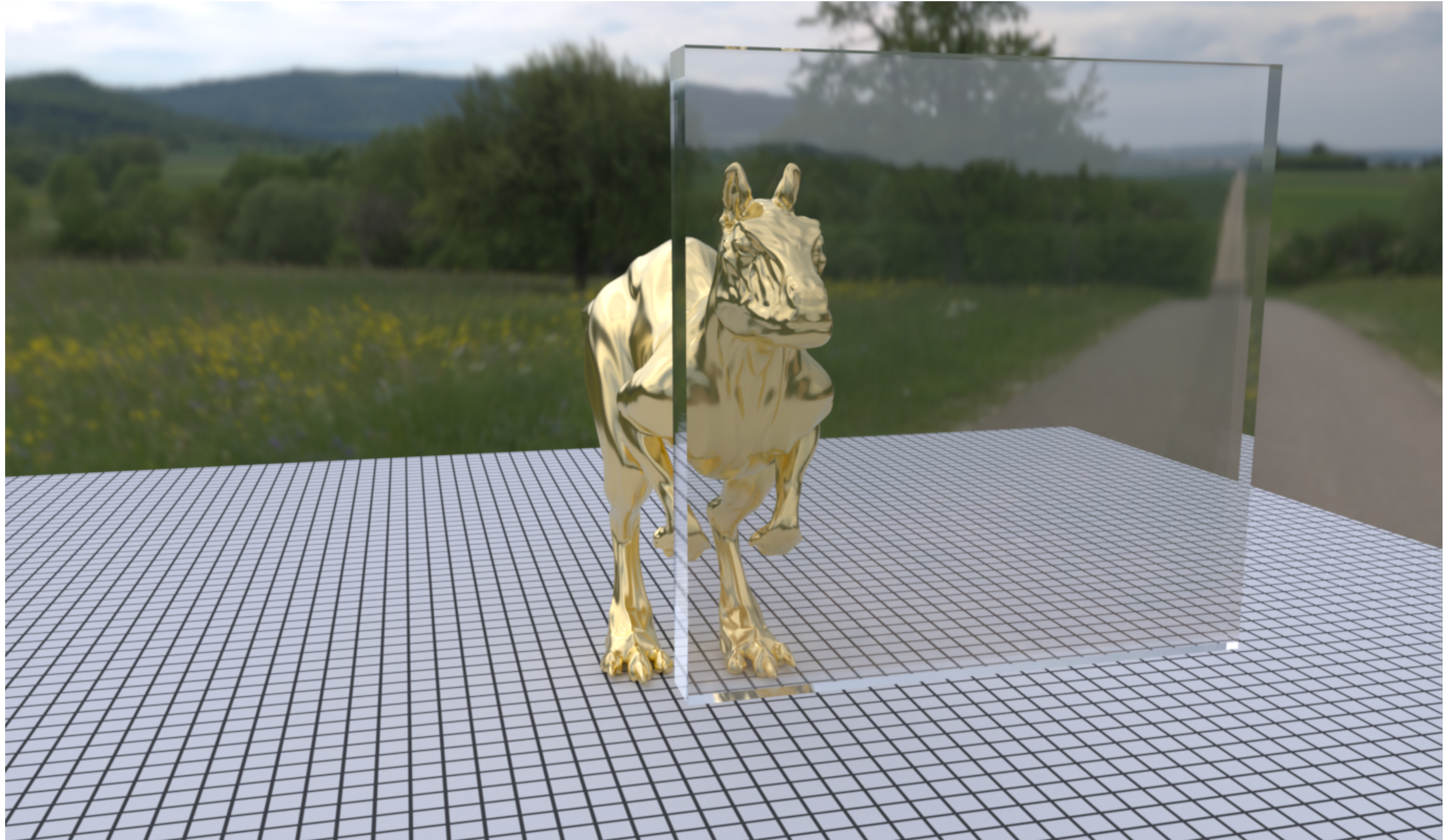
Thin vs Thick Glass



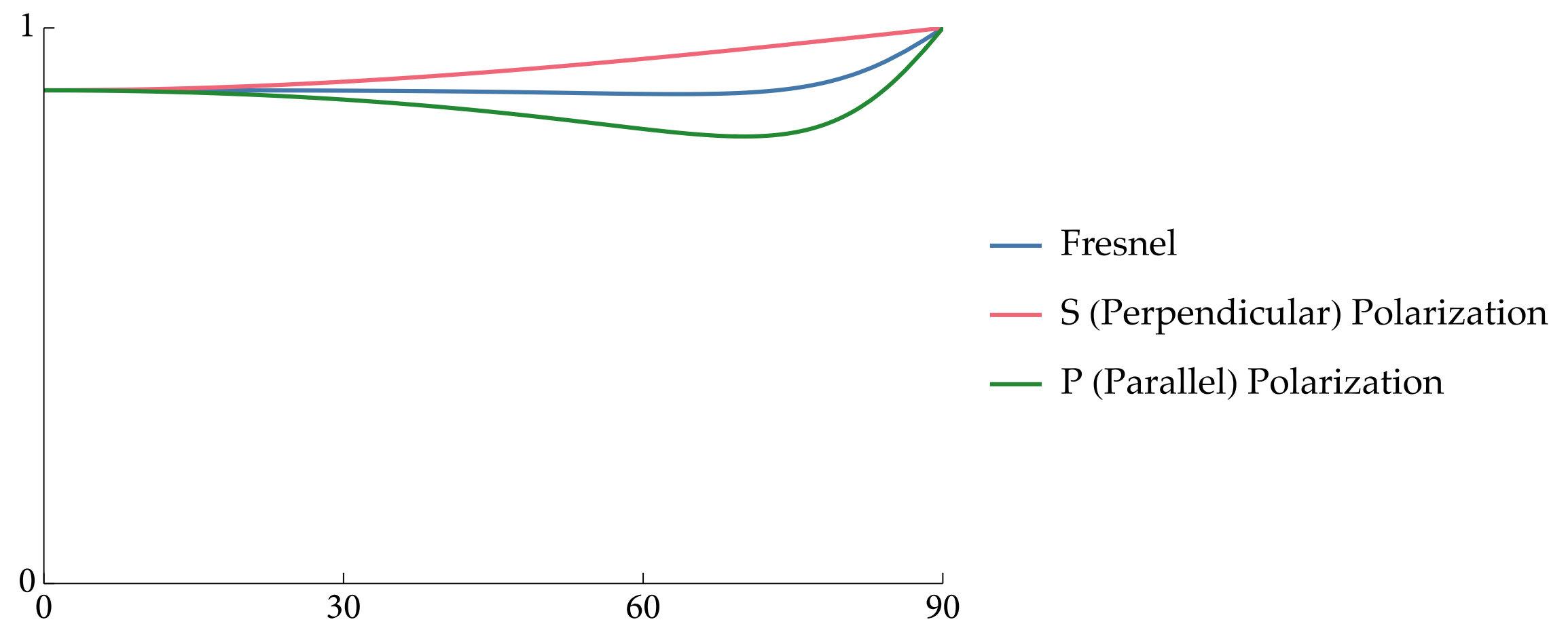
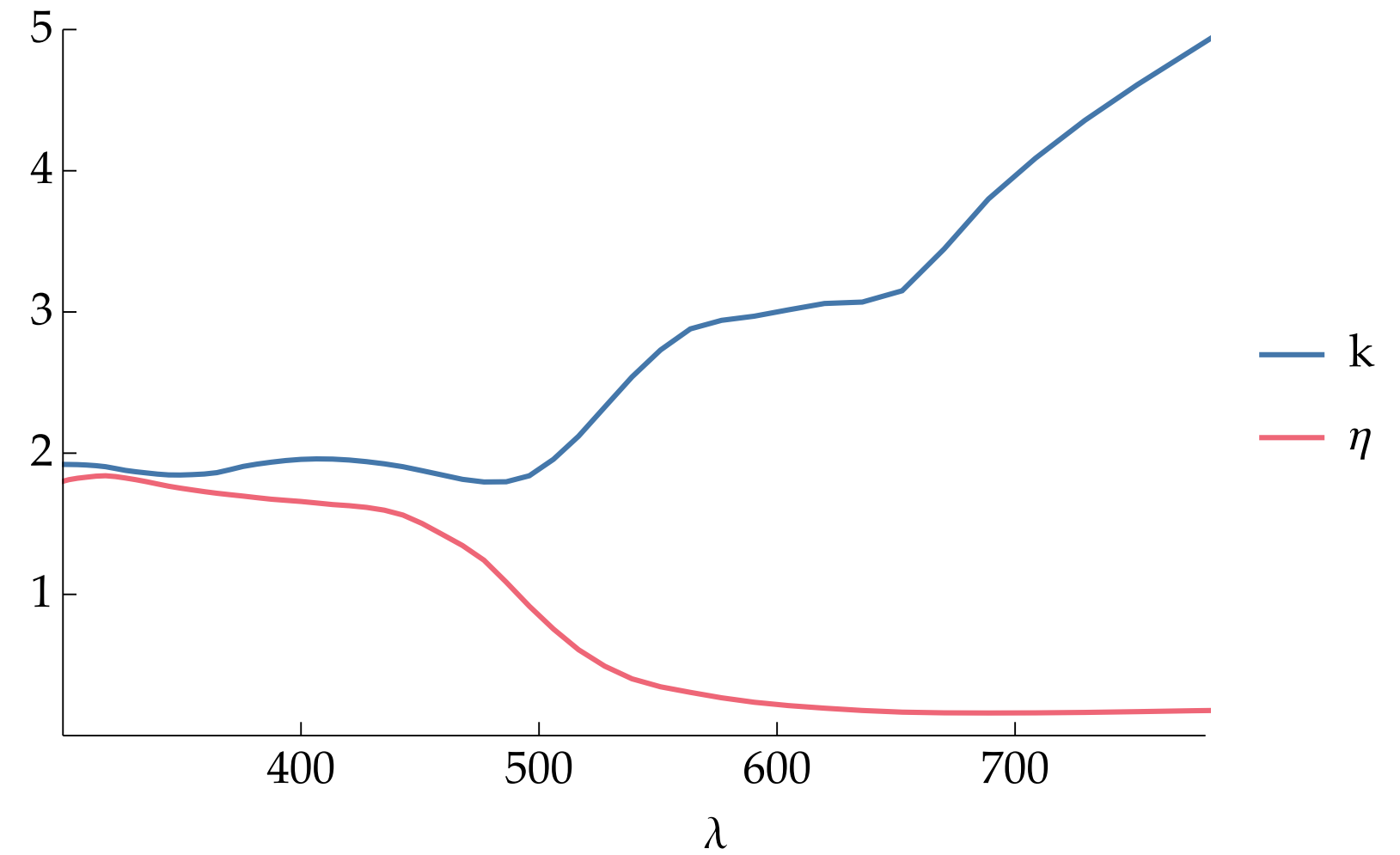
Thin Glass



Thick Glass

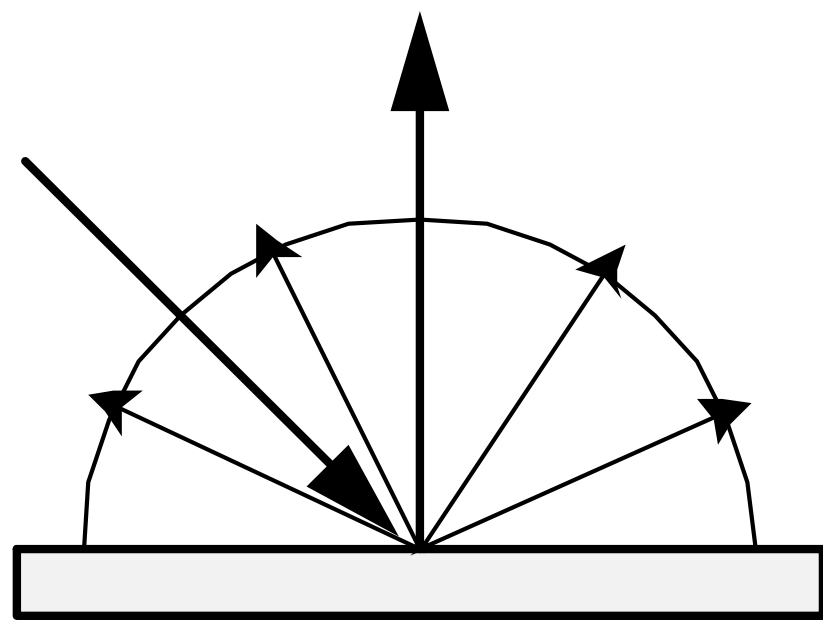


Fresnel Conductor: Gold



Ideal Diffuse Reflection

Assume light is equally likely to be reflected in any output direction



$$f_{r,d} = c$$

$$\begin{aligned} L_o(\omega_o) &= \int f_r L_i(\omega_i) \cos \theta_i d\omega_i \\ &= f_r \int L_i(\omega_i) \cos \theta_i d\omega_i \\ &= f_r E \end{aligned}$$

$$\begin{aligned} \rho_d &= \frac{\int L_o(\omega_o) \cos \theta_o d\omega_o}{\int L_i(\omega_i) \cos \theta_i d\omega_i} = \frac{L_o \int \cos \theta_o d\omega_o}{E} \\ &= \frac{L_o \pi}{E} = \frac{f_o E \pi}{E} = \pi f_r \quad \longrightarrow \quad \boxed{f_r = \frac{\rho_d}{\pi}} \end{aligned}$$

“Diffuse” Reflection

Theoretical

- **Bouguer - Special micro-facet distribution**
- **Seeliger - Subsurface reflection**
- **Multiple surface or subsurface reflections**

Experimental

- **Pressed magnesium oxide powder**
- **Almost never valid at high angles of incidence**

Paint manufactures attempt to create ideal diffuse

Experiment

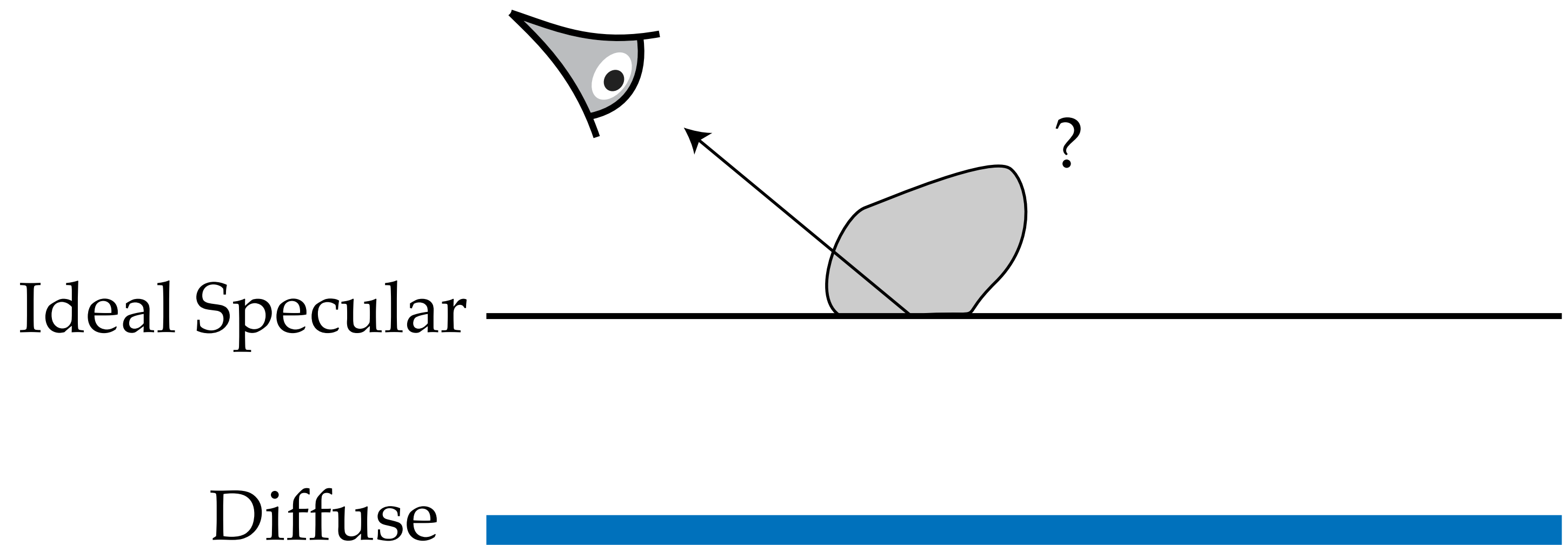
Reflections from a shiny floor



From Lafortune, Foo, Torrance, Greenberg, SIGGRAPH 97

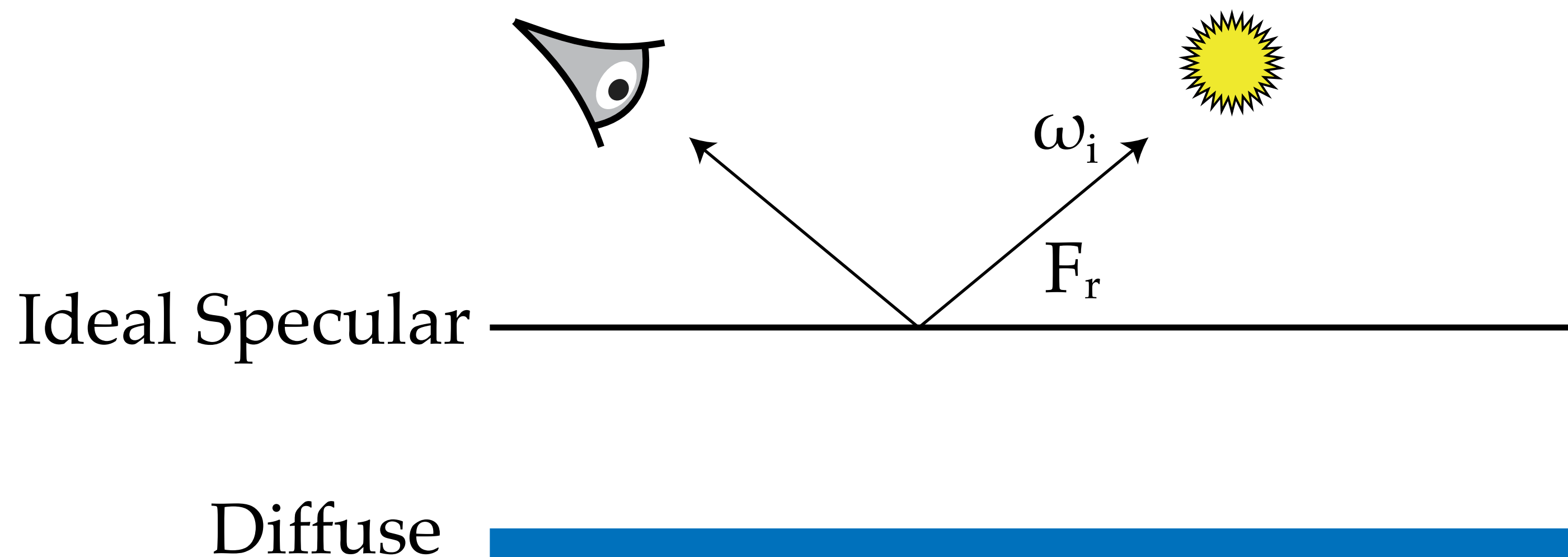
Reflection is greater at glancing angles

Coated Diffuse BRDF



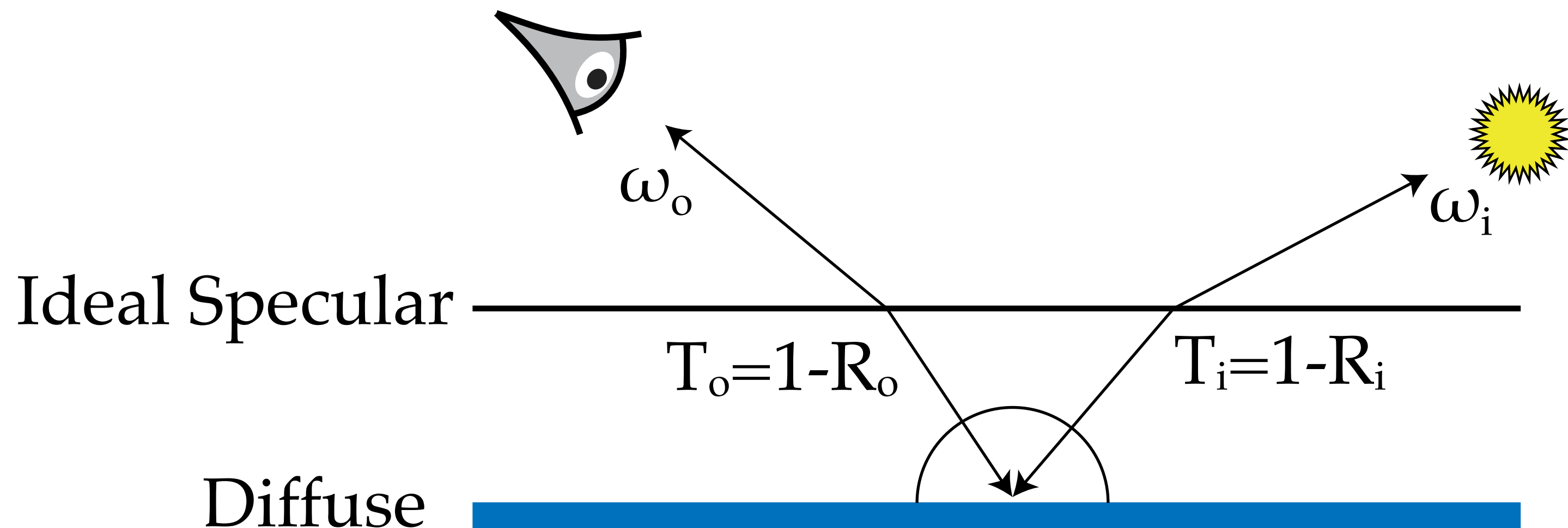
Coated Diffuse BRDF

$$f_r(\omega_o \rightarrow \omega_i) = F_r(\omega_i) \frac{\delta(\omega_i - R(\omega_o, \mathbf{n}))}{\cos \theta_i} + \dots$$

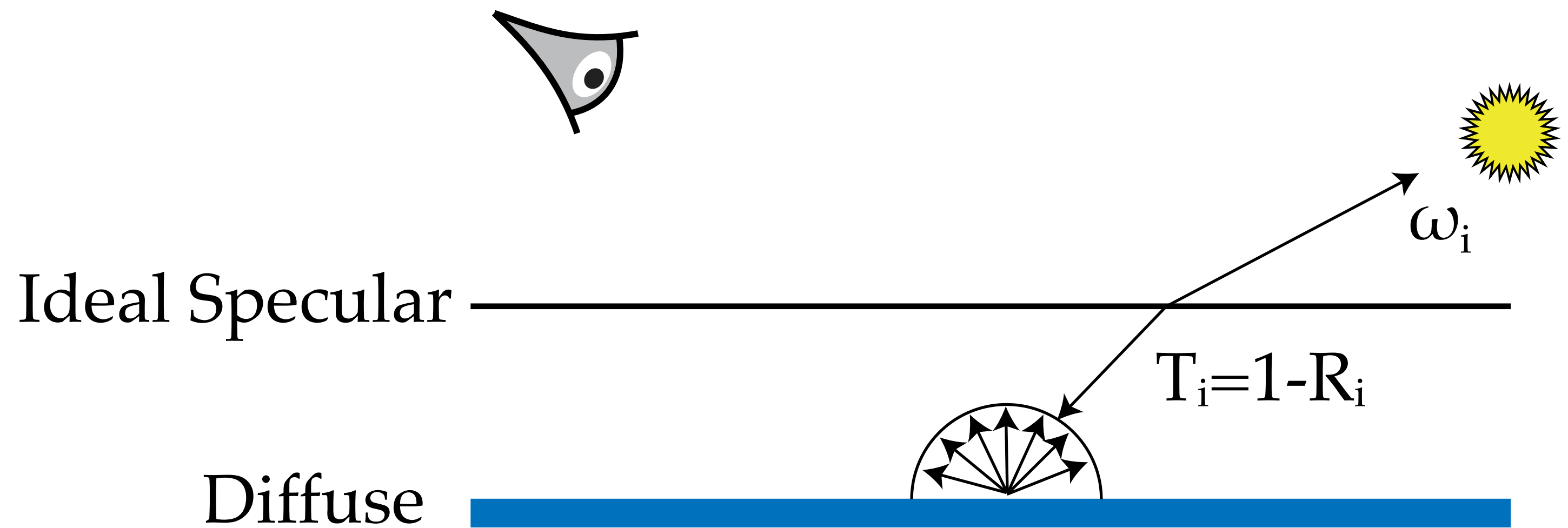


Coated Diffuse BRDF

$$f_r(\omega_o \rightarrow \omega_i) = F_r(\omega_i) \frac{\delta(\omega_i - R(\omega_o, \mathbf{n}))}{\cos \theta_i} + (1 - F_r(\omega_o)) \frac{\rho_d}{\pi} (1 - F_r(\omega_i)) + \dots$$



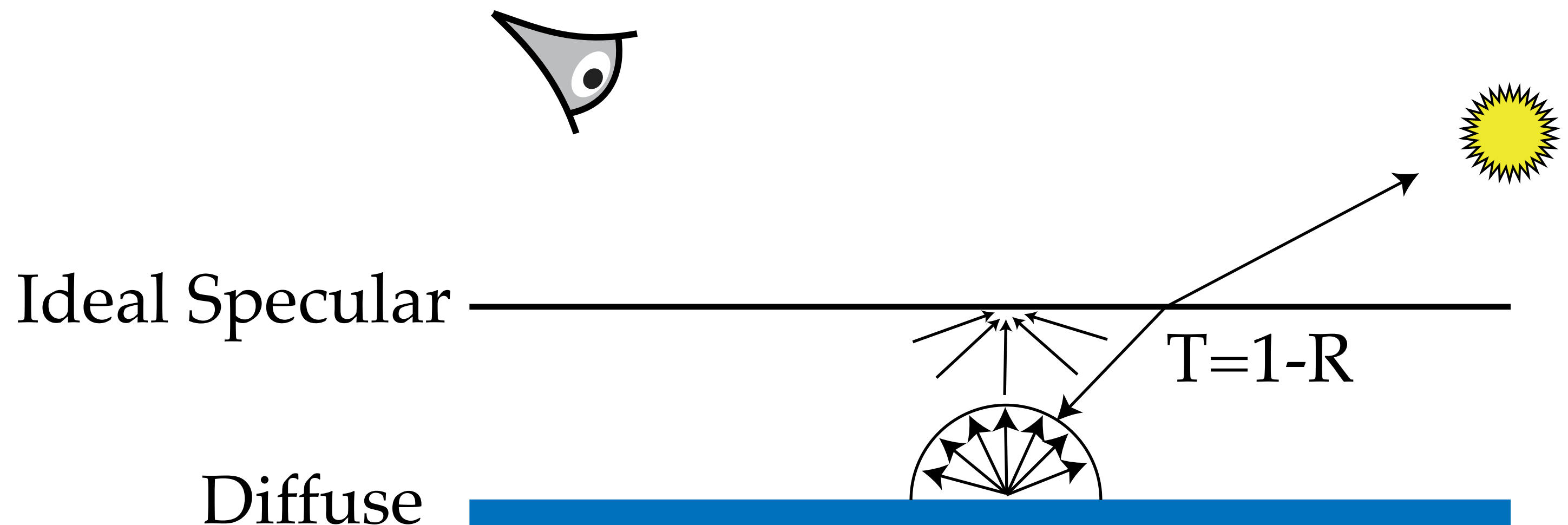
Coated Diffuse BRDF



Coated Diffuse BRDF

How much light is reflected downward at the interface?

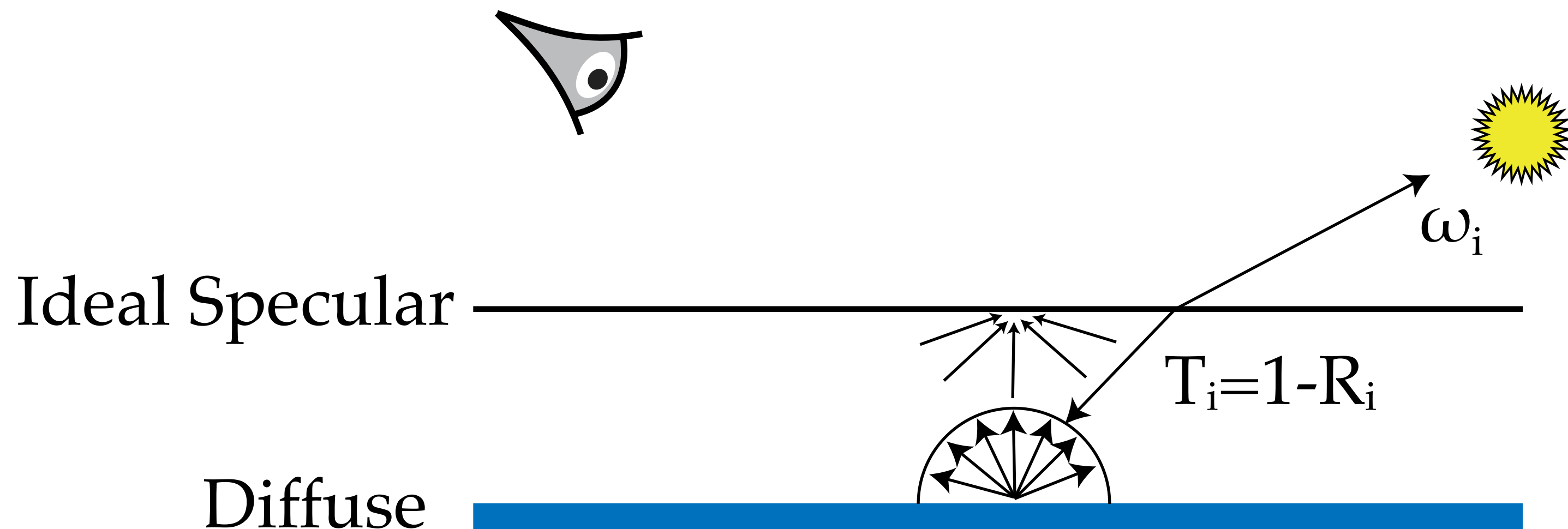
$$\tilde{r} = \int_{\Omega} F_r(\omega, \eta) d\omega$$



Coated Diffuse BRDF

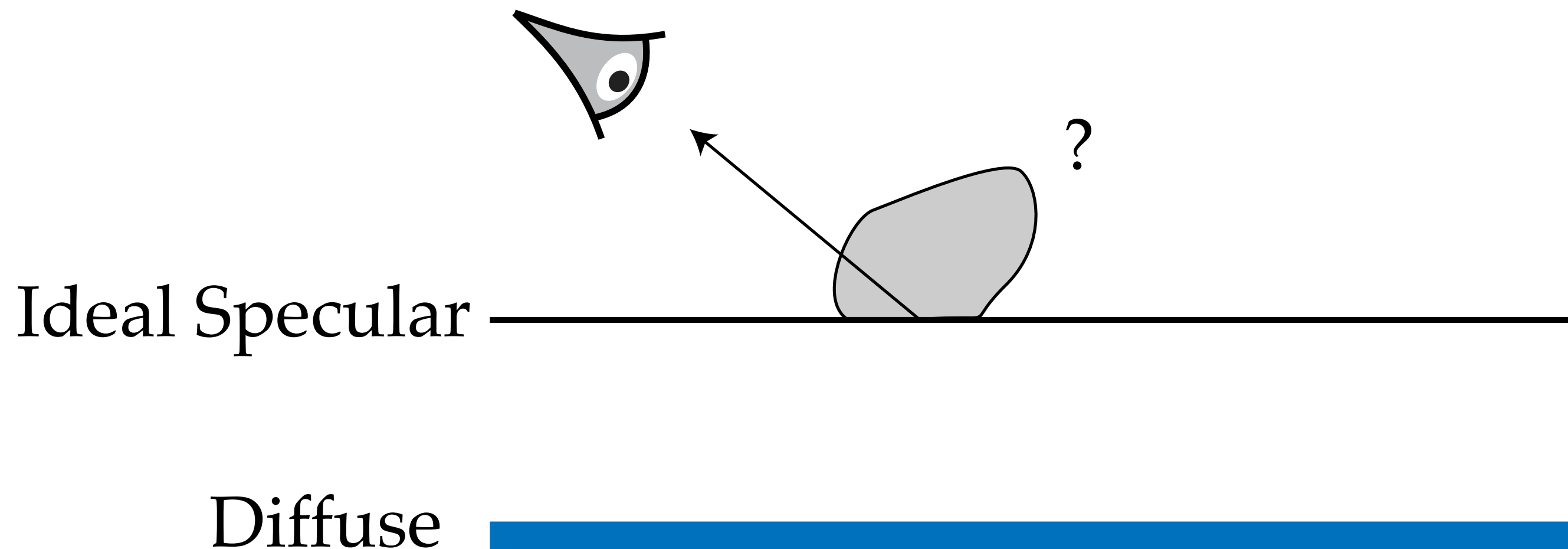
Inter-reflection inside the layer:

$$f_r + f_r \tilde{r} f_r + f_r \tilde{r} f_r \tilde{r} f_r + \dots = \frac{f_r}{1 - \tilde{r} f_r}$$

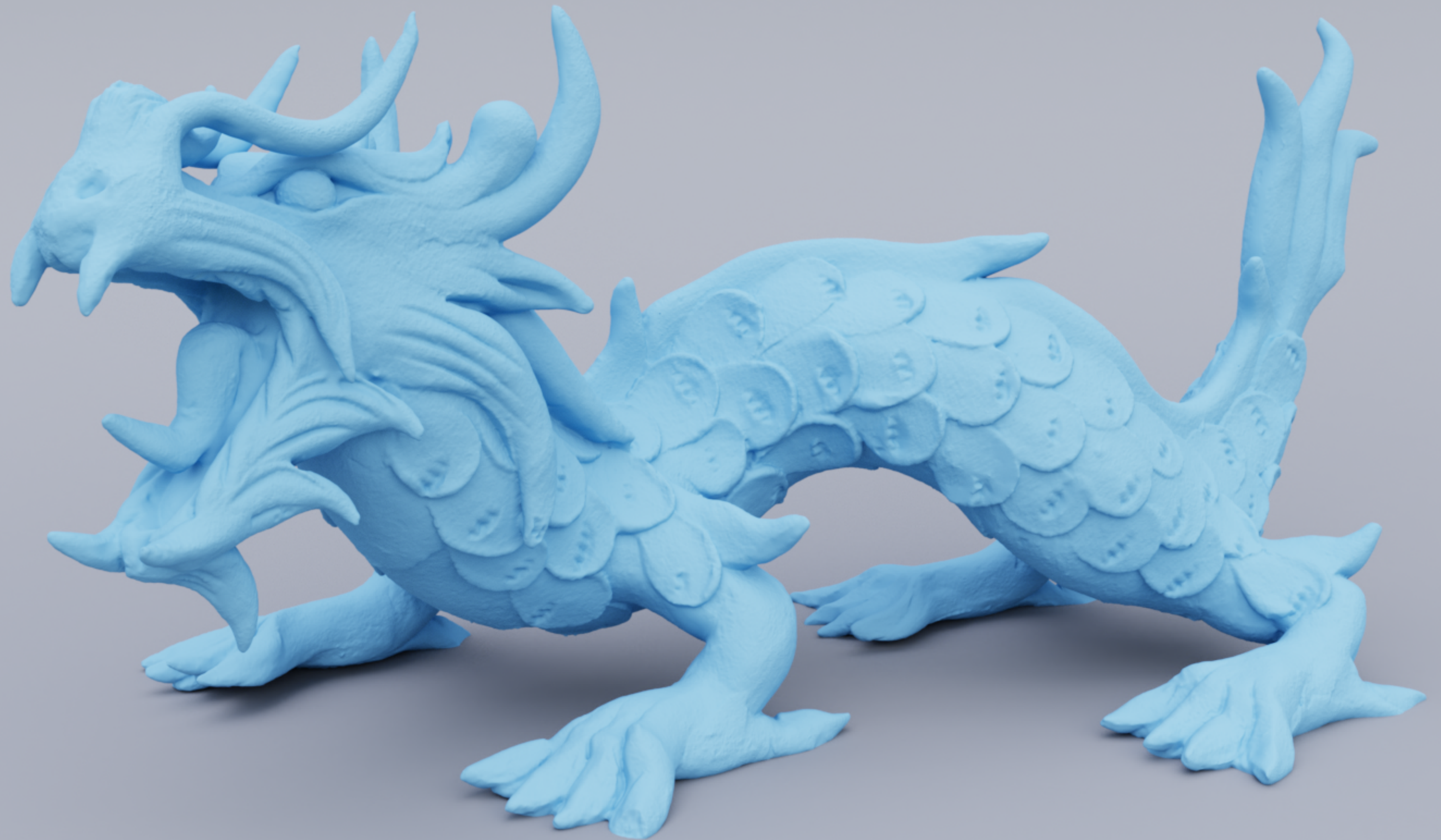


Coated Diffuse BRDF

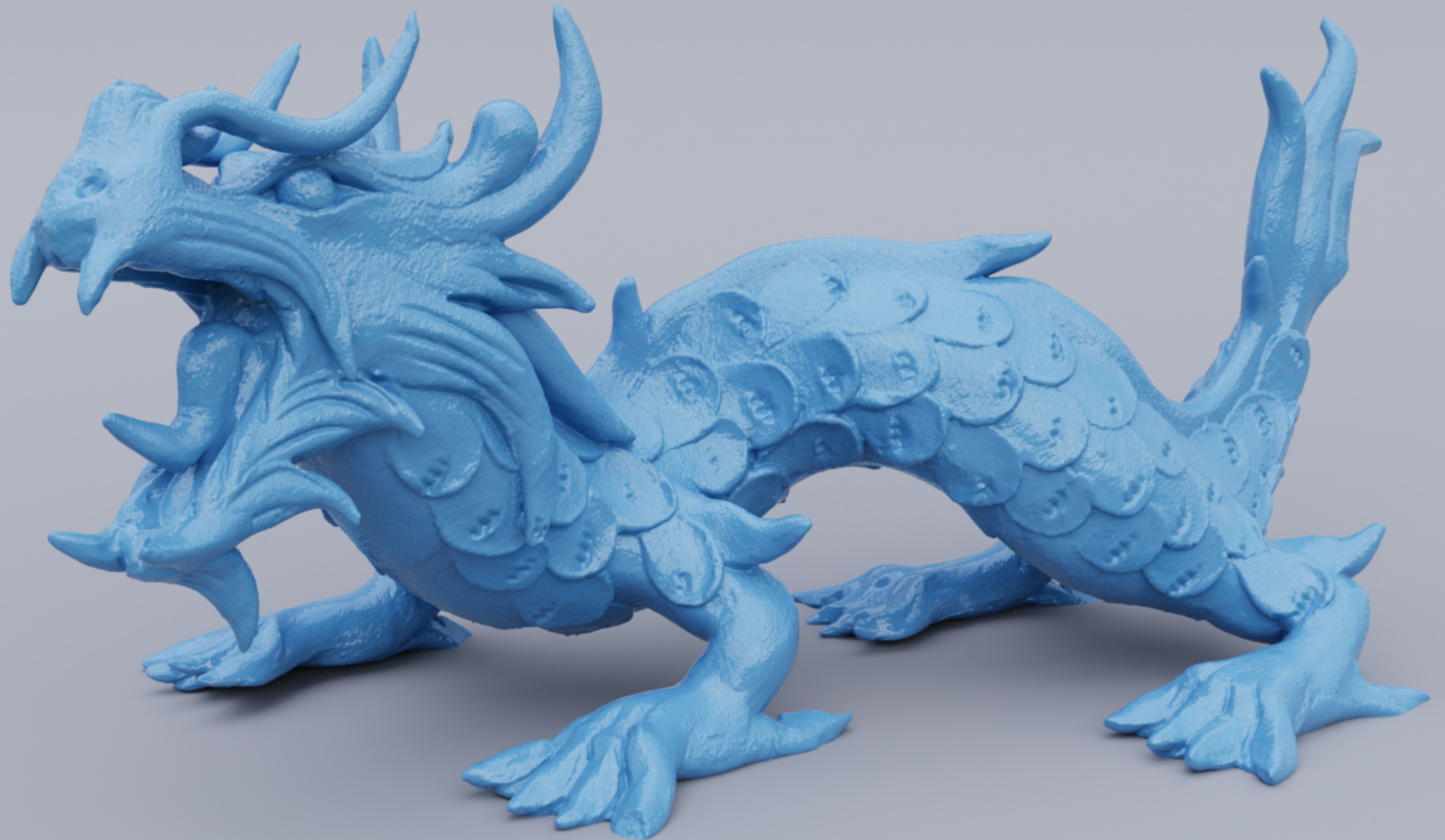
$$f_r(\omega_o \rightarrow \omega_i) = F_r(\omega_i) \frac{\delta(\omega_i - R(\omega_o, \mathbf{n}))}{\cos \theta_i} + (1 - F_r(\omega_o)) \frac{f_r}{1 - \tilde{r} f_r} (1 - F_r(\omega_i))$$



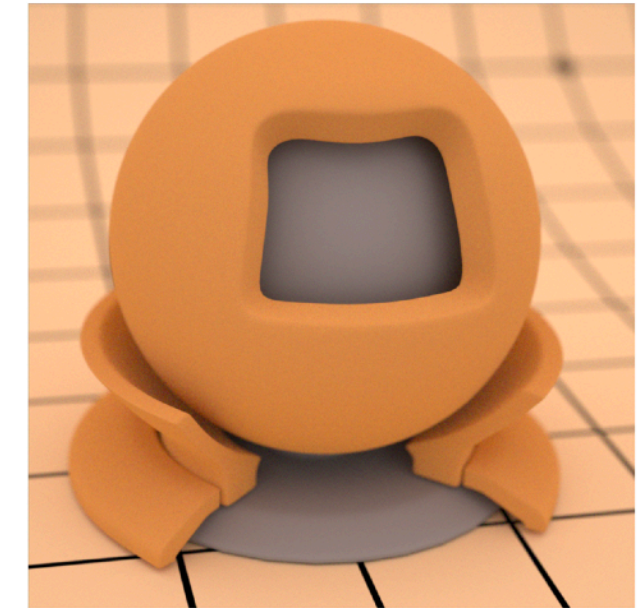
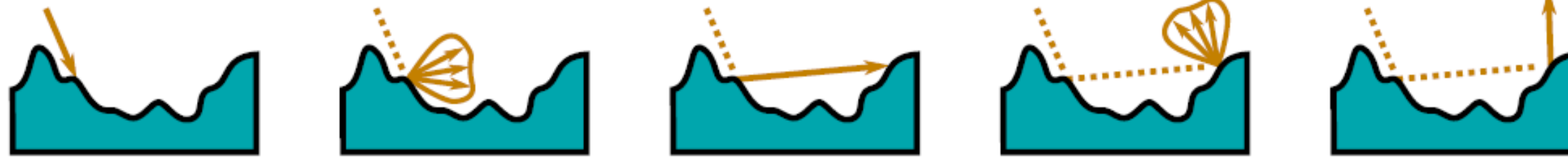
Diffuse BRDF



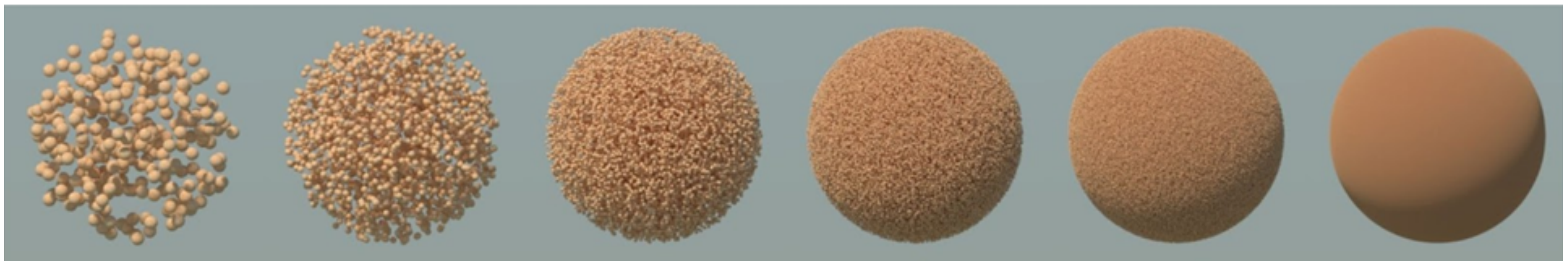
Coated Diffuse BRDF



Lambertian Generalizations



Heitz, E. et al. 2016. *Multiple-Scattering Microfacet BSDFs with the Smith Model.*



d'Eon, E. 2021. *An Analytic BRDF for Materials with Spherical Lambertian Scatterers.*

BRDF follow from inserting Equation 15 into the general solution [HC61, p.55], and we find

$$\begin{aligned}\Psi^{(0)}(\mu) &= \frac{1}{384}c \left(-15(c-1)(4c+9)\mu^4 + (c(20c+281) - 346)\mu^2 + 207 \right), \\ \Psi^{(1)}(\mu) &= -\frac{1}{192}c (\mu^2 - 1) (5(4c+9)\mu^2 - 64), \\ \Psi^{(2)}(\mu) &= \frac{15}{256}c (\mu^2 - 1)^2.\end{aligned}$$

We can then numerically evaluate the H functions using the

Fok/Chandrasekhar equation [Foc44, Kre62]

$$H^{(i)}(\mu) = \exp \left(-\frac{\mu}{\pi} \int_0^\infty \frac{1}{1+\mu^2 t^2} \log K^{(i)}(t) dt \right), \quad (22)$$

where the functions $K^{(i)}(t)$ are given by [Kre62]

$$K^{(i)}(t) = 1 - \int_1^\infty \left(\frac{1}{s-it} + \frac{1}{s+it} \right) \frac{\Psi^{(i)}\left(\frac{1}{s}\right)}{s} ds. \quad (23)$$

Working these out, we find

$$K^{(0)}(t) = 1 - \frac{c \left((256c - 301)t^3 + \left((346 - c(20c + 281))t^2 - 15(c-1)(4c+9) + 207t^4 \right) \tan^{-1}(t) + 15(c-1)(4c+9)t \right)}{192t^5}, \quad (24)$$

$$K^{(1)}(t) = 1 - \frac{c \left((40c + 282)t^3 - 3(t^2 + 1) \left(20c + 64t^2 + 45 \right) \tan^{-1}(t) + 15(4c+9)t \right)}{288t^5}, \quad (25)$$

$$K^{(2)}(t) = 1 - \frac{5c \left(3(t^2 + 1)^2 \tan^{-1}(t) - t(5t^2 + 3) \right)}{128t^5}. \quad (26)$$

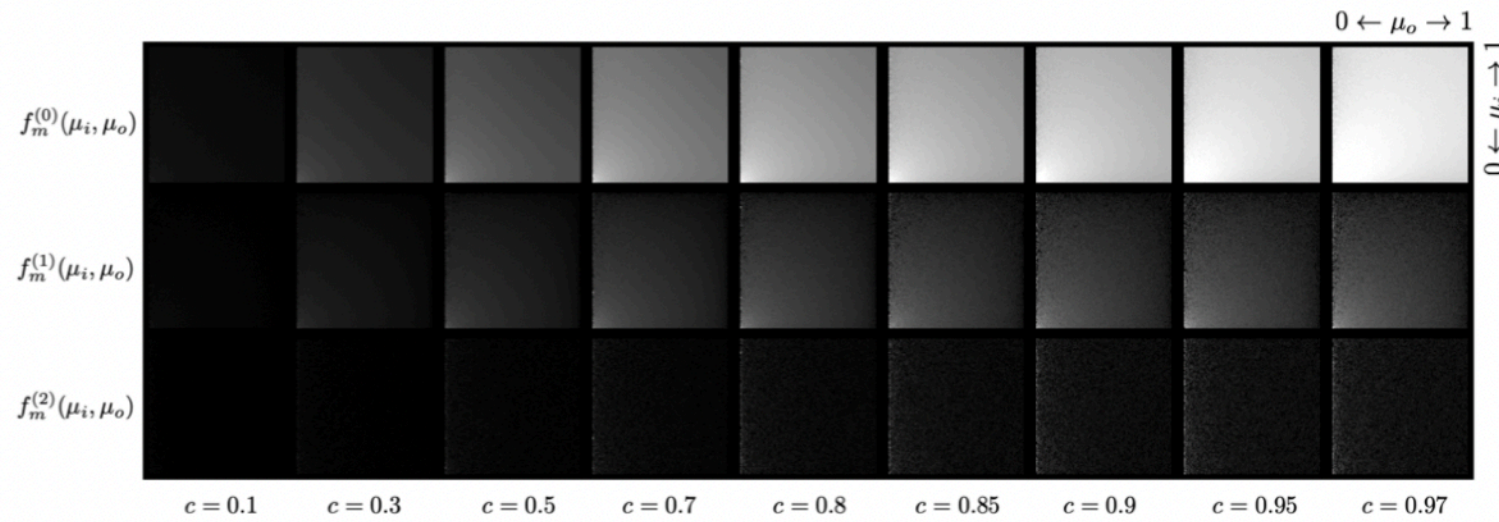


Figure 3: Using Monte Carlo reference, we observe comparatively weak signal in the second-order mode of the multiple-scattering portion of the BRDF, $f^{(2)}(\mu_i, \mu_o)$ (bottom row).

3.3. First-order Fourier mode

In Figure 3 we see that the first-order Fourier mode $f_m^{(1)}$ of the multiple scattering is non-negligible. This requires that f_m has a term of the form $f(\mu_i, \mu_o) \cos(\phi)$ for some function f . We approximate this term from the exact solution and this one of the key differences of our BRDF to previous approximations, which assume $f_m^{(1)} = 0$ [Hap81, Hap02].

The exact first-order mode of the BRDF is [HC61, Eq.(43)]

$$\begin{aligned}f^{(1)}(\mu_i, \mu_o) &= \frac{cH^{(1)}(\mu_i)H^{(1)}(\mu_o)}{6\pi(\mu_i + \mu_o)} \sqrt{(1-\mu_i^2)(1-\mu_o^2)} \times \\ &\quad \times \left(1 + \left(l^2 + \frac{45m}{64} \right) \mu_i \mu_o + l(\mu_i + \mu_o) \right), \quad (27)\end{aligned}$$